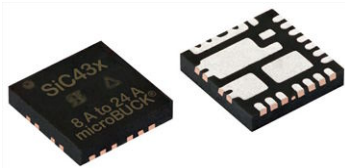


3 V to 28 V Input, 8 A, 12 A microBUCK® DC/DC Converter



LINKS TO ADDITIONAL RESOURCES



DESCRIPTION

The SiC43x are synchronous buck regulators with integrated high side and low side power MOSFETs. Its power stage is capable of supplying 12 A (SiC437) and 8 A (SiC438) continuous current at up to 1 MHz switching frequency. This regulator produces an adjustable output voltage down to 0.6 V from 3 V to 28 V input rail to accommodate a variety of applications, including computing, consumer electronics, telecom, and industrial.

SiC437's and SiC438's architecture delivers ultrafast transient response with minimum output capacitance and tight ripple regulation at very light load. The device is internally compensated and is stable with any capacitor. No external ESR network is required for loop stability purposes. The device also incorporates a power saving scheme that significantly increases light load efficiency.

The regulator family integrates a full protection feature set, including output overvoltage protection (OVP), cycle by cycle overcurrent protection (OCP) short circuit protection (SCP) and thermal shutdown (OTP). It also has UVLO and a user programmable soft start.

The SiC437 and SiC438 are available in lead (Pb)-free power enhanced MLP-44L package in 4 mm x 4 mm dimension.

APPLICATIONS

- 5 V, 12 V, and 24 V input rail POLs
- Desktop, notebooks, server, and industrial computing
- Industrial and automation
- consumer electronics

TYPICAL APPLICATION CIRCUIT AND PACKAGE OPTIONS

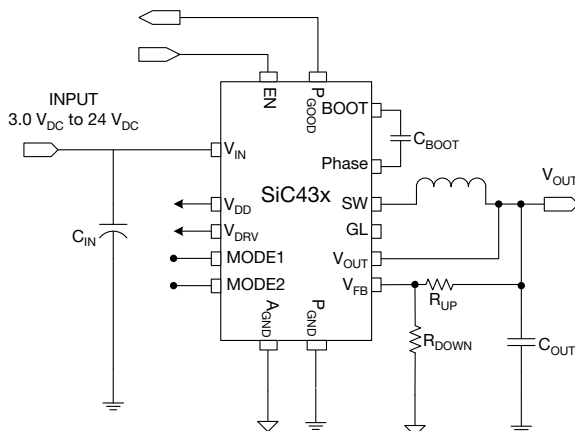


Fig. 1 - Typical Application Circuit

FEATURES

- Versatile
 - Operation from 3 V to 28 V input voltage
 - Adjustable output voltage down to 0.6 V
 - Scalable solution 8 A (SiC438), 12 A (SiC437), and 24 A (SiC431)
 - Output voltage tracking and sequencing with pre-bias start up
 - $\pm 1\%$ output voltage accuracy at $-40\text{ }^{\circ}\text{C}$ to $+125\text{ }^{\circ}\text{C}$
- Highly efficient
 - 97 % peak efficiency
 - 1 μA supply current at shutdown
 - 50 μA operating current not switching
- Highly configurable
 - Four programmable switching frequencies available: 300 kHz, 500 kHz, 750 kHz, and 1 MHz
 - Adjustable soft start and adjustable current limit
 - Three modes of operation: forced continuous conduction, power save (SiC43xB, SiC43xD), or ultrasonic (SiC43xA, SiC43xC)
- Robust and reliable
 - Cycle-by-cycle current limit
 - Output overvoltage protection
 - Output undervoltage / short circuit protection with auto retry
 - Power good flag and over temperature protection
- Material categorization: for definitions of compliance please see www.vishay.com/doc?99912



RoHS
COMPLIANT
HALOGEN
FREE

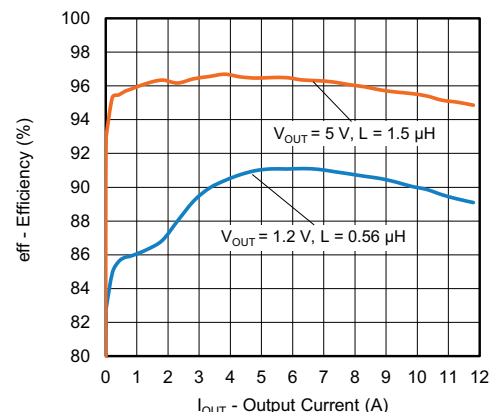
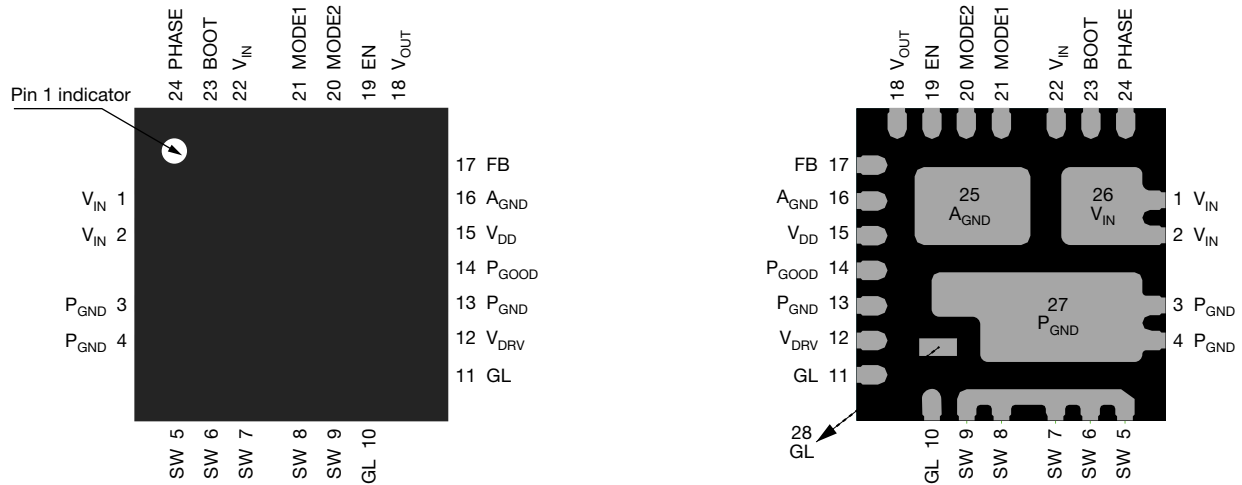


Fig. 2 - Efficiency vs. Output Current
($V_{IN} = 12\text{ V}$, $f_{sw} = 500\text{ kHz}$, Power Saving Mode)

PIN CONFIGURATION

Fig. 3 - SiC43x Pin Configuration

| PIN DESCRIPTION | | |
|-----------------|------------|---|
| PIN NUMBER | SYMBOL | DESCRIPTION |
| 1, 2, 22, 26 | V_{IN} | Input voltage |
| 3, 4, 13, 27 | P_{GND} | Power signal return ground |
| 5 to 9 | SW | Switching node signal; output inductor connection point |
| 10, 11, 28 | GL | Low side power MOSFET gate signal |
| 12 | V_{DRV} | Supply voltage for internal gate driver. Connect a 2.2 μF decoupling capacitor to P_{GND} |
| 14 | P_{GOOD} | Power good signal output; open drain |
| 15 | V_{DD} | Supply voltage for internal logic. Connect a 1 μF decoupling capacitor to A_{GND} |
| 16, 25 | A_{GND} | Analog signal return ground |
| 17 | FB | Output voltage feedback pin; connect to V_{OUT} through a resistor divider network. |
| 18 | V_{OUT} | Output voltage sense pin |
| 19 | EN | Enable pin |
| 20 | MODE2 | Soft start and current limit selection; connect a resistor to V_{DD} or A_{GND} per table 2 |
| 21 | MODE1 | Operating mode and switching frequency selection; connect a resistor to V_{DD} or A_{GND} per table 1 |
| 23 | BOOT | Bootstrap pin; connect a capacitor to PHASE pin for HS power MOSFET gate voltage supply |
| 24 | PHASE | Switching node signal for bootstrap return path |

| ORDERING INFORMATION | | | | | | |
|----------------------|--------------|-----------------|----------------------|-----------------|--------------------------------|---------------------|
| PART NUMBER | PART MARKING | MAXIMUM CURRENT | V_{DD} , V_{DRV} | LIGHT LOAD MODE | OPERATING JUNCTION TEMPERATURE | PACKAGE |
| SiC437AED-T1-GE3 | SiC437A | 12 A | Internal | Ultrasonic | -40 °C to +125 °C | PowerPAK® MLP44-24L |
| SiC437BED-T1-GE3 | SiC437B | | | Power saving | | |
| SiC437CED-T1-GE3 | SiC437C | | External | Ultrasonic | | |
| SiC437DED-T1-GE3 | SiC437D | | | Power saving | | |
| SiC438AED-T1-GE3 | SiC438A | 8 A | Internal | Ultrasonic | | |
| SiC438BED-T1-GE3 | SiC438B | | | Power saving | | |
| SiC438CED-T1-GE3 | SiC438C | | External | Ultrasonic | | |
| SiC438DED-T1-GE3 | SiC438D | | | Power saving | | |



| ABSOLUTE MAXIMUM RATINGS ($T_A = 25\text{ }^\circ\text{C}$, unless otherwise noted) | | | |
|--|--|--------------|---------------------------|
| ELECTRICAL PARAMETER | CONDITIONS | LIMITS | UNIT |
| V_{IN} | Reference to P_{GND} | -0.3 to +30 | V |
| V_{OUT} | Reference to P_{GND} | -0.3 to +22 | |
| V_{DD} / V_{DRV} | Reference to P_{GND} | -0.3 to +6 | |
| SW / PHASE | Reference to P_{GND} | -0.3 to +30 | |
| SW / PHASE (AC) | 100 ns; reference to P_{GND} | -8 to +35 | |
| BOOT | Reference to P_{GND} | -0.3 to +6 | |
| BOOT to SW | | -0.3 to +6 | |
| A_{GND} to P_{GND} | | -0.3 to +0.3 | |
| EN | Reference to A_{GND} | -0.3 to +30 | |
| All other pins | Reference to A_{GND} | -0.3 to +6 | |
| Temperature | | | |
| Junction temperature | T_J | -40 to +150 | $^\circ\text{C}$ |
| Storage temperature | T_{STG} | -65 to +150 | |
| Power Dissipation | | | |
| Junction to ambient thermal impedance ($R_{\theta JA}$) | | 16 | $^\circ\text{C}/\text{W}$ |
| Junction to case thermal impedance ($R_{\theta JC}$) | | 2 | |
| Maximum power dissipation | Ambient temperature = $25\text{ }^\circ\text{C}$ | 7.75 | W |
| ESD Protection | | | |
| Electrostatic discharge protection | Human body model | 4000 | V |
| | Charged device model | 1000 | |

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating/conditions for extended periods may affect device reliability.

| RECOMMENDED OPERATING CONDITIONS (all voltages referenced to GND = 0 V) | | | | |
|--|------|-------------|--|------------------|
| PARAMETER | MIN. | TYP. | MAX. | UNIT |
| Input voltage (V_{IN}) (SiC43xA, SiC43xB) | 4.5 | - | 28 | V |
| Input voltage (V_{IN}) (SiC43xC, SiC43xD) | 3 | - | 28 | |
| Logic supply voltage, gate driver supply voltage (V_{DD} , V_{DRV}) (SiC43xC, SiC43xD) | 4.5 | - | 28 | |
| Enable (EN) | 0 | - | 28 | |
| Input voltage (V_{IN}), external supply on V_{DD} / V_{DRV} | 3 | - | 28 | |
| Output voltage (V_{OUT}) | 0.6 | - | $0.9 \times V_{IN}$ and $< 20\text{ V}$ | |
| Temperature | | | | |
| Recommended ambient temperature | | -40 to +105 | | $^\circ\text{C}$ |
| Operating junction temperature | | -40 to +125 | | |

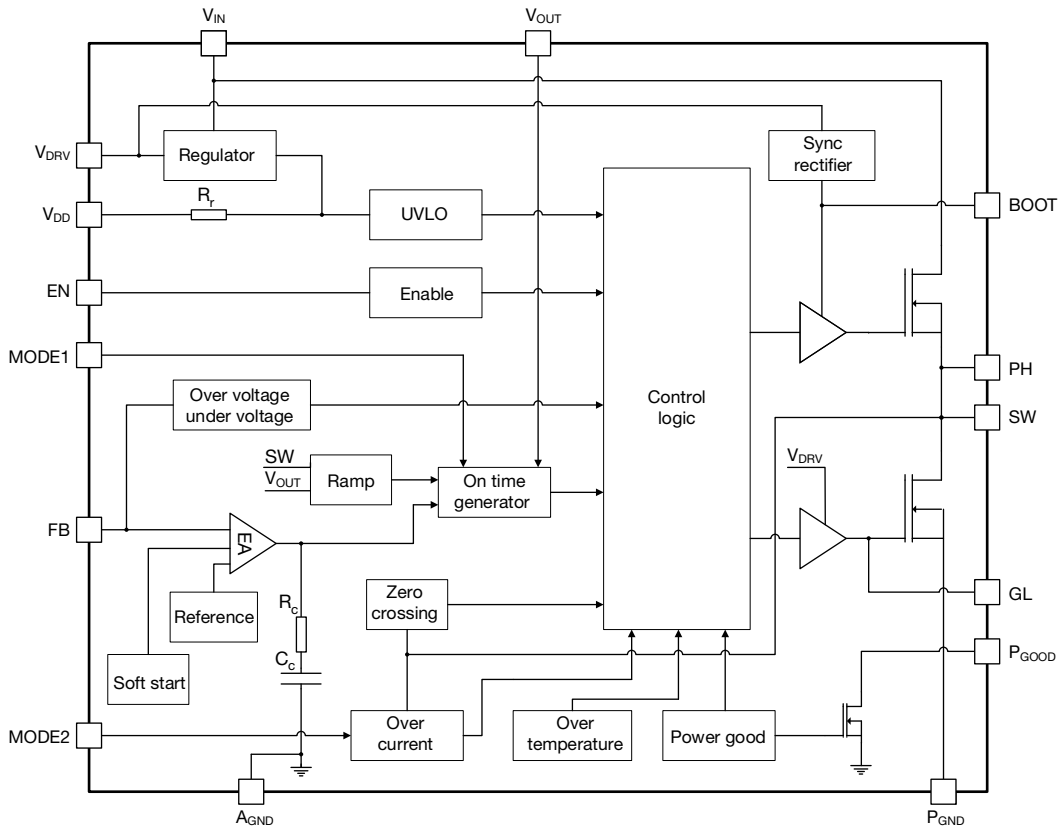


| ELECTRICAL SPECIFICATIONS ($V_{IN} = 12\text{ V}$, $V_{EN} = 5\text{ V}$, $T_J = -40\text{ }^\circ\text{C}$ to $+125\text{ }^\circ\text{C}$, unless otherwise stated) | | | | | | |
|--|----------------------------|---|------|------|------|------------------|
| PARAMETER | SYMBOL | TEST CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| Power Supplies | | | | | | |
| V_{DD} supply | V_{DD} | $V_{IN} = 6\text{ V to }28\text{ V}$ (SiC43xA, SiC43xB) | 4.75 | 5 | 5.25 | V |
| V_{DD} UVLO threshold, rising | V_{DD_UVLO} | | 3.3 | 3.6 | 3.9 | |
| V_{DD} UVLO hysteresis | $V_{DD_UVLO_HYST}$ | | - | 300 | - | mV |
| Maximum V_{DD} current | I_{DD} | $V_{IN} = 6\text{ V to }28\text{ V}$ | 3 | - | - | mA |
| V_{DRV} supply | V_{DRV} | $V_{IN} = 6\text{ V to }28\text{ V}$ (SiC43xA, SiC43xB) | 4.75 | 5 | 5.25 | V |
| Maximum V_{DRV} current | I_{DRV} | $V_{IN} = 6\text{ V to }28\text{ V}$ | 50 | - | - | mA |
| Input current | I_{VIN} | Non-switching, $V_{FB} > 0.6\text{ V}$ | - | 50 | 120 | μA |
| Shutdown current | I_{VIN_SHDN} | $V_{EN} = 0\text{ V}$ | - | 0.5 | 3 | |
| Controller and Timing | | | | | | |
| Feedback voltage | V_{FB} | $T_J = 25\text{ }^\circ\text{C}$ | 597 | 600 | 603 | mV |
| | | $T_J = -40\text{ }^\circ\text{C to }+125\text{ }^\circ\text{C}^{(1)}$ | 594 | 600 | 606 | |
| V_{FB} input bias current | I_{FB} | | - | 2 | - | nA |
| Minimum on-time | $t_{ON_MIN.}$ | | - | 50 | 65 | ns |
| t_{ON} accuracy | $t_{ON_ACCURACY}$ | | -10 | - | 10 | % |
| On-time range | t_{ON_RANGE} | | 65 | - | 2250 | ns |
| Minimum frequency, skip mode | $f_{SW_MIN.}$ | Ultrasonic version (SiC43xA, SiC43xC) | 20 | - | 30 | kHz |
| | | Power save version (SiC43xB, SiC43xD) | 0 | - | - | |
| Minimum off-time | $t_{OFF_MIN.}$ | | 205 | 250 | 305 | ns |
| Power MOSFETs (SiC437) | | | | | | |
| High side on resistance | R_{ON_HS} | $V_{DRV} = 5\text{ V}$, $T_A = 25\text{ }^\circ\text{C}$ | - | 10.1 | - | m Ω |
| Low side on resistance | R_{ON_LS} | | - | 3.9 | - | |
| Power MOSFETs (SiC438) | | | | | | |
| High side on resistance | R_{ON_HS} | $V_{DRV} = 5\text{ V}$, $T_A = 25\text{ }^\circ\text{C}$ | - | 10.1 | - | m Ω |
| Low side on resistance | R_{ON_LS} | | - | 5.5 | - | |
| Fault Protections | | | | | | |
| Over current protection (inductor valley current) | I_{OCL_P} | $T_J = -10\text{ }^\circ\text{C to }+125\text{ }^\circ\text{C}$ | -20 | - | 20 | % |
| Output OVP threshold | V_{OVP} | V_{FB} with respect to 0.6 V reference | - | 20 | - | |
| Output UVP threshold | V_{UVP} | | - | -80 | - | |
| Over temperature protection | T_{OTP_RISING} | Rising temperature | - | 150 | - | $^\circ\text{C}$ |
| | T_{OTP_HYST} | Hysteresis | - | 25 | - | |
| Power Good | | | | | | |
| Power good output threshold | $V_{FB_RISING_VTH_OV}$ | V_{FB} rising above 0.6 V reference | - | 20 | - | % |
| | $V_{FB_FALLING_VTH_UV}$ | V_{FB} falling below 0.6 V reference | - | -10 | - | |
| Power good hysteresis | V_{FB_HYST} | | - | 40 | - | mV |
| Power good on resistance | R_{ON_PGOOD} | | - | 7.5 | 15 | Ω |
| Power good delay time | t_{DLY_PGOOD} | | 15 | 25 | 35 | μs |
| EN / MODE / Ultrasonic Threshold | | | | | | |
| EN logic high level | V_{EN_H} | | 1.6 | - | - | V |
| EN logic low level | V_{EN_L} | | - | - | 0.4 | |
| EN pull down resistance | R_{EN} | | - | 5 | - | M Ω |
| Switching Frequency | | | | | | |
| MODE1 (switching frequency) | R_{MODE1} | $f_{sw} = 300\text{ kHz}$ | - | 51 | 55 | k Ω |
| | | $f_{sw} = 500\text{ kHz}$ | 90 | 100 | 110 | |
| | | $f_{sw} = 750\text{ kHz}$ | 180 | 200 | 220 | |
| | | $f_{sw} = 1000\text{ kHz}$ | 450 | 499 | 550 | |

| ELECTRICAL SPECIFICATIONS ($V_{IN} = 12\text{ V}$, $V_{EN} = 5\text{ V}$, $T_J = -40\text{ }^\circ\text{C}$ to $+125\text{ }^\circ\text{C}$, unless otherwise stated) | | | | | | |
|--|-------------|--|------|------|------|------------|
| PARAMETER | SYMBOL | TEST CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| Soft Start | | | | | | |
| Soft start time | t_{ss} | Connect R_{MODE2} between MODE2 and AGND | 1.8 | 3 | 4.2 | ms |
| | | Connect R_{MODE2} between MODE2 and V_{DD} | 3.6 | 6 | 8.4 | |
| Over Current Protection - SiC437 | | | | | | |
| MODE 2 (over current protection) | R_{MODE2} | $I_{OCP} = 18\text{ A}$ | 450 | 499 | 550 | k Ω |
| | | $I_{OCP} = 14\text{ A}$ | 180 | 200 | 220 | |
| | | $I_{OCP} = 9.7\text{ A}$ | 90 | 100 | 110 | |
| | | $I_{OCP} = 5.4\text{ A}$ | - | 51 | 55 | |
| Over Current Protection - SiC438 | | | | | | |
| MODE 2 (over current protection) | R_{MODE2} | $I_{OCP} = 12\text{ A}$ | 450 | 499 | 550 | k Ω |
| | | $I_{OCP} = 9.3\text{ A}$ | 180 | 200 | 220 | |
| | | $I_{OCP} = 6.5\text{ A}$ | 90 | 100 | 110 | |
| | | $I_{OCP} = 3.6\text{ A}$ | - | 51 | 55 | |

Note

(1) Guaranteed by design

FUNCTIONAL BLOCK DIAGRAM

Fig. 4 - SiC43x Functional Block Diagram

OPERATIONAL DESCRIPTION

Device Overview

The SiC43x is high efficiency synchronous buck regulators capable of delivering up to 8 A (SiC438) and 12 A (SiC437) continuous current. The device has user programmable switching frequency of 300 kHz, 500 kHz, 750 kHz, and 1 MHz. The control scheme delivers fast transient response and minimizes the number of external components. Thanks to the internal ramp information, no high ESR output bulk or virtual ESR network is required for the loop stability. This device also incorporates a power saving feature that enables diode emulation mode and frequency fold back as the load decreases.

SiC43x has a full set of protection and monitoring features:

- Over current protection in pulse-by-pulse mode
- Output over voltage protection
- Output under voltage protection with device latch
- Over temperature protection with hysteresis
- Dedicated enable pin for easy power sequencing
- Power good open drain output

This device is available in MLP44-24L package to deliver high power density and minimize PCB area.

Power Stage

SiC43x integrates a high performance power stage with a low on resistance and gate charge, high side and low side MOSFETs. The MOSFETs are optimized to achieve up to 97 % efficiency.

The input voltage (V_{IN}) can go up to 28 V and down to as low as 3 V for power conversion. For input voltages (V_{IN}) below 4.5 V an external V_{DD} and V_{DRV} supply is required (SiC43xC, SiC43xD). For input voltages (V_{IN}) above 4.5 V only a single input supply is required (SiC43xA, SiC43xB).

Control Mechanism

SiC43x employs an advanced voltage - mode COT control mechanism. During steady-state operation, feedback voltage (V_{FB}) is compared with internal reference (0.6 V typ.) and the amplified error signal (V_{COMP}) is generated at the internal comp node. An internally generated ramp signal and V_{COMP} feed into a comparator. Once V_{RAMP} crosses V_{COMP} , an on-time pulse is generated for a fixed time. During the on-time pulse, the high side MOSFET will be turned on. Once the on-time pulse expires, the low side MOSFET will be turned on after a dead time period. The low side MOSFET will stay on for a minimum duration equal to the minimum off-time ($t_{OFF_MIN.}$) and remains on until V_{RAMP} crosses V_{COMP} . The cycle is then repeated.

Fig. 5 illustrates the basic block diagram for VM-COT architecture. In this architecture the following is achieved:

- The reference of a basic ripple control regulator is replaced with a high gain error amplifier loop
- This establishes two parallel voltage regulating feedback paths, a fast and slow path
- Fast path is the ripple injection which ensures rapid correction of the transient perturbation

- Slow path is the error amplifier loop which ensures the DC component of the output voltage follows the internal accurate reference voltage

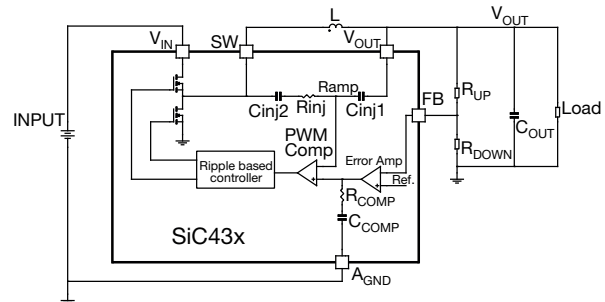


Fig. 5 - VM-COT Block Diagram

All components for RAMP signal generation and error amplifier compensation required for the control loop are internal to the IC, see Fig. 5. In order for the device to cover a wide range of V_{OUT} operation, the internal RAMP signal components (R_X , C_X , C_Y) are automatically selected depending on the V_{OUT} voltage and switching frequency. This method allows the RAMP amplitude to remain constant throughout the V_{OUT} voltage range, achieving low jitter and fast transient Response. The error amplifier internal compensation consists of a resistor in series with a capacitor (R_{COMP} , C_{COMP}).

Fig. 6 demonstrates the basic operational waveforms:

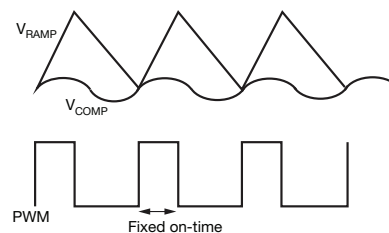


Fig. 6 - VM-COT Operational Principle

Light Load Condition

To improve efficiency at light-load condition, SiC437, SiC438 provide a set of innovative implementations to eliminate LS recirculating current and switching losses. The internal zero crossing detector monitors SW node voltage to determine when inductor current starts to flow negatively. In power saving mode, as soon as inductor valley current crosses zero, the device deploys diode emulation mode by turning off low side MOSFET. If load further decreases, switching frequency is reduced proportional to load condition to save switching losses while keeping output ripple within tolerance. The switching frequency is set by the controller to maintain regulation. In the standard power save mode, there is no minimum switching frequency (SiC43xB, SiC43xD). For SiC43xA, SiC43xC, the minimum switching frequency that the regulator will reduce to is > 20 kHz as the part avoids switching frequencies in the audible range. This light load mode implementation is called ultrasonic mode.

MODE SETTING, OVER CURRENT PROTECTION, SWITCHING FREQUENCY, AND SOFT START SELECTION

The SiC437, SiC438 has a low pin count, minimal external components, and offers the user flexibility to choose soft start times, current limit settings, switching frequencies and to enable or disable the light load mode. Two MODE pins,

MODE1 and MODE2, are user programmable by connecting a resistor from MODEx to V_{DD} or A_{GND}, allowing the user to choose various operating modes. This is best explained in the tables below.

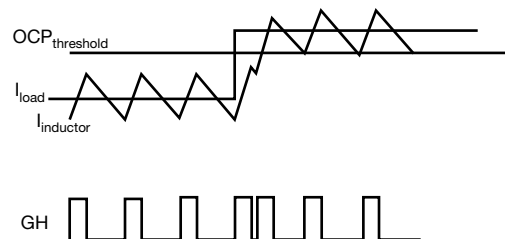
| TABLE 1 - MODE1 CONFIGURATION SETTINGS | | | |
|---|---------------------|---------------------------|-------------------------|
| OPERATION | CONNECTION | f _{SWITCH} (kHz) | R _{MODE1} (kΩ) |
| Skip | to A _{GND} | 300 | 51 |
| | | 500 | 100 |
| | | 750 | 200 |
| | | 1000 | 499 |
| Forced CCM | to V _{DD} | 300 | 51 |
| | | 500 | 100 |
| | | 750 | 200 |
| | | 1000 | 499 |

| TABLE 2 - MODE2 CONFIGURATION SETTINGS | | | |
|---|---------------------|--|-------------------------|
| SOFT-START TIME | CONNECTION | I _{LIMIT} (%) | R _{MODE2} (kΩ) |
| 3 ms | to A _{GND} | 30 | 51 |
| | | 54 | 100 |
| | | 78 | 200 |
| | | 100 % (18 A on SiC437) 100 % (12 A on SiC438) | 499 |
| 6 ms | to V _{DD} | 30 | 51 |
| | | 54 | 100 |
| | | 78 | 200 |
| | | 100 % (18 A on SiC437) 100 % (12 A on SiC438) | 499 |

OUTPUT MONITORING AND PROTECTION FEATURES
Output Overcurrent Protection (OCP)

SiC437, SiC438 has pulse-by-pulse over current limit control. The inductor current is monitored during low side MOSFET conduction time through R_{DS(on)} sensing. After a pre-defined blanking time, the inductor current is compared with an internal OCP threshold. If inductor current is higher than OCP threshold, high side MOSFET is kept off until the inductor current falls below OCP threshold.

OCP is enabled immediately after V_{DD} passes UVLO rising threshold.


Fig. 7 - Over-Current Protection Illustration

Output Undervoltage Protection (UVP)

UVP is implemented by monitoring the FB pin. If the voltage level at FB drops below 0.12 V for more than 25 μ s, a UVP event is recognized and both high side and low side MOSFETs are turned off. After a duration equivalent to 20 soft start periods, the IC attempts to re-start. If the fault condition still exists, the above cycle will be repeated.

UVP is active after the completion of soft start sequence.

Output Overvoltage Protection (OVP)

OVP is implemented by monitoring the FB pin. If the voltage level at FB rising above 0.72 V, a OVP event is recognized and both high side and low side MOSFETs are turned off. Normal operation is resumed once FB voltage drop below 0.68 V.

OOVP is active after V_{DD} passes UVLO rising threshold.

Over-Temperature Protection (OTP)

OTP is implemented by monitoring the junction temperature. If the junction temperature rises above 150 $^{\circ}$ C, a OTP event is recognized and both high side and low MOSFETs are turned off. After the junction temperature falls below 125 $^{\circ}$ C (25 $^{\circ}$ C hysteresis), the device restarts by initiating a soft start sequence.

Sequencing of Input / Output Supplies

SiC437, SiC438 have no sequencing requirements on its supplies or enables (V_{IN} , V_{DD} , V_{DRV} , EN).

Enable

The SiC437, SiC438 have an enable pin to turn the part on and off.

Driving the pin high enables the device, while driving the pin low disables the device.

The EN pin is internally pulled to A_{GND} by a 5 M Ω resistor to prevent unwanted turn on due to a floating GPIO.

Pre-Bias Start-Up

In case of pre-bias startup, output is monitored through FB pin. If the sensed voltage on FB is higher than the internal reference ramp value, control logic prevents high side and low side MOSFETs from switching to avoid negative output voltage spike and excessive current sinking through low side MOSFET.

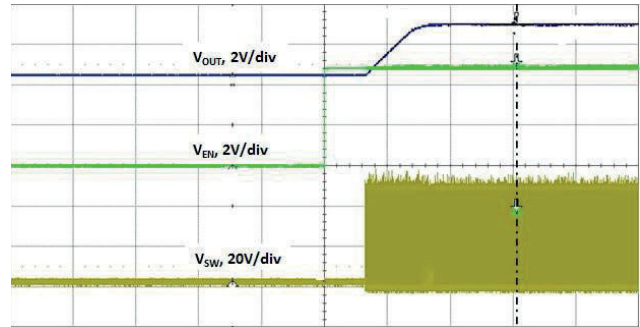


Fig. 8 - Pre-Bias Start-Up

Power Good

SiC437, SiC438 power good is an open-drain output. Pull P_{GOOD} pin high through a > 10 k Ω resistor to use this signal. Power good window is shown in the below diagram. If voltage on FB pin is out of this window, P_{GOOD} signal is de-asserted by pulling down to A_{GND} . To prevent false triggering during transient events, P_{GOOD} has a 25 μ s blanking time.

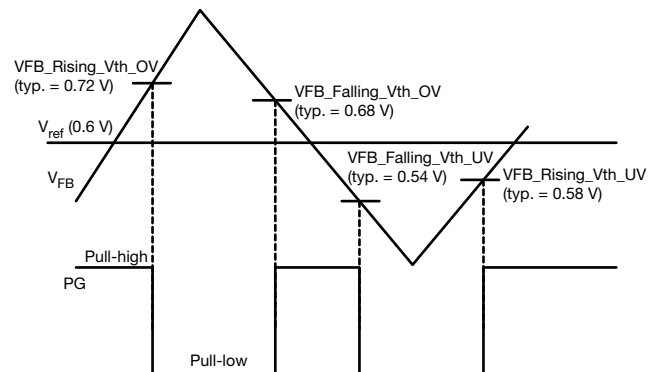


Fig. 9 - P_{GOOD} Window Diagram

ELECTRICAL CHARACTERISTICS

($V_{IN} = 12\text{ V}$, $V_{OUT} = 1.2\text{ V}$, $f_{sw} = 500\text{ kHz}$, $C_{OUT} = 47\text{ }\mu\text{F} \times 7$, $C_{IN} = 10\text{ }\mu\text{F} \times 6$, unless otherwise noted)

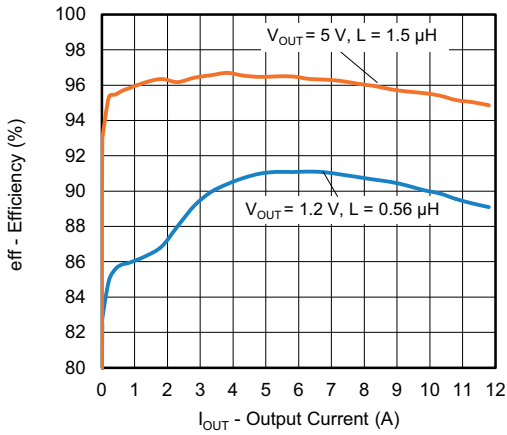


Fig. 10 - SiC437 Efficiency vs. Output Current
($V_{IN} = 12\text{ V}$, $f_{sw} = 500\text{ kHz}$, Full Load)

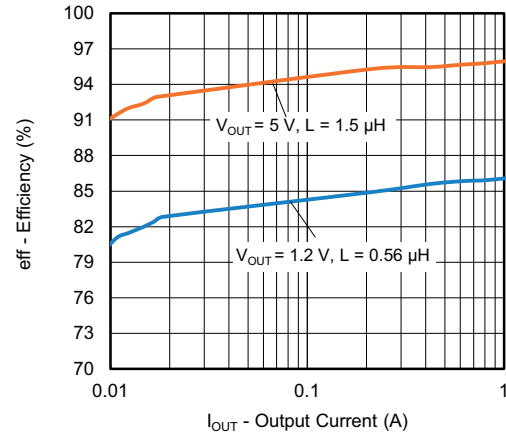


Fig. 13 - SiC437 Efficiency vs. Output Current
($V_{IN} = 12\text{ V}$, $f_{sw} = 500\text{ kHz}$, Light Load)

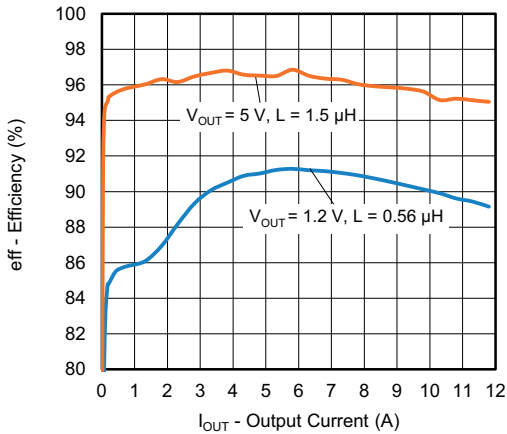


Fig. 11 - SiC437 Efficiency vs. Output Current
($V_{IN} = 12\text{ V}$, $f_{sw} = 500\text{ kHz}$, Ultrasonic Mode, Full Load)

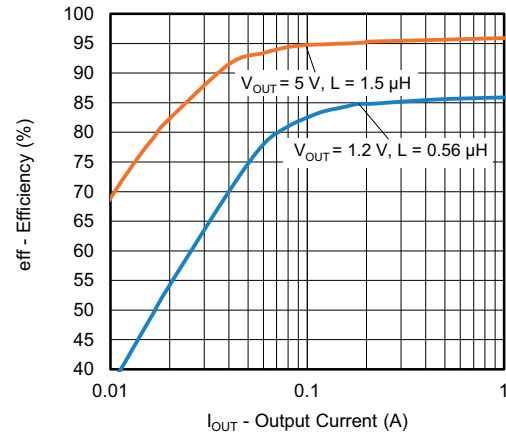


Fig. 14 - SiC437 Efficiency vs. Output Current
($V_{IN} = 12\text{ V}$, $f_{sw} = 500\text{ kHz}$, Ultrasonic Mode, Light Load)

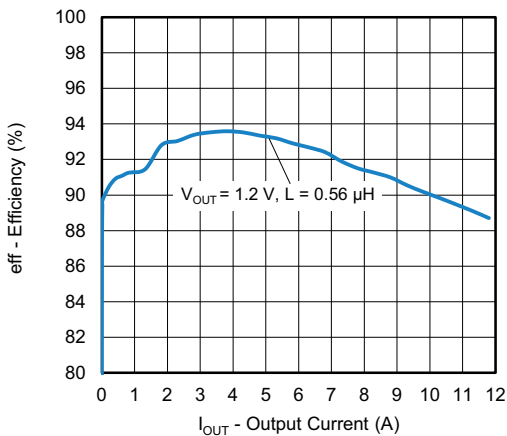


Fig. 12 - SiC437 Efficiency vs. Output Current
($V_{IN} = 5\text{ V}$, $f_{sw} = 500\text{ kHz}$, Full Load)

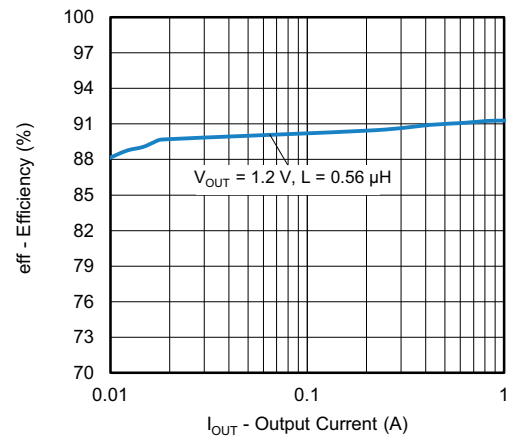


Fig. 15 - SiC437 Efficiency vs. Output Current
($V_{IN} = 5\text{ V}$, $f_{sw} = 500\text{ kHz}$, Light Load)



ELECTRICAL CHARACTERISTICS

(VIN = 12 V, VOUT = 1.2 V, fsw = 500 kHz, COUT = 47 μF x 7, CIN = 10 μF x 6, unless otherwise noted)

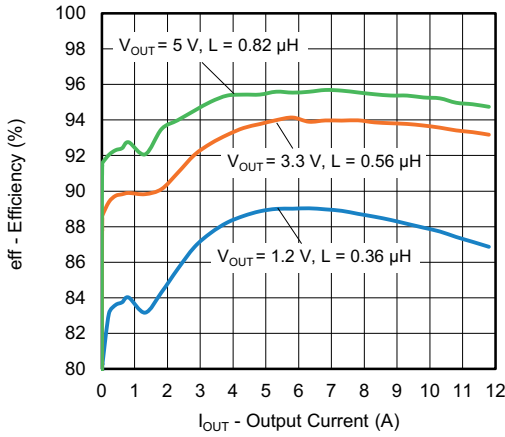


Fig. 16 - SiC437 Efficiency vs. Output Current (VIN = 12 V, fsw = 1 MHz, Full Load)

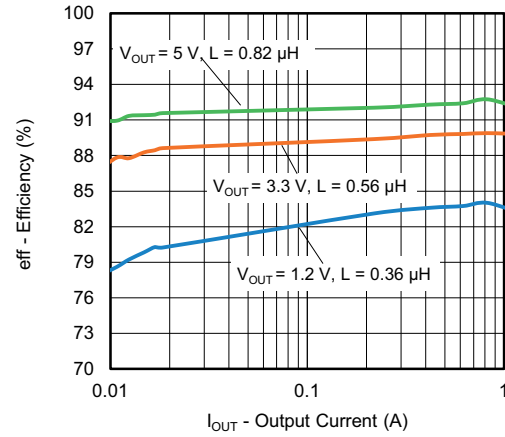


Fig. 19 - SiC437 Efficiency vs. Output Current (VIN = 12 V, fsw = 1 MHz, Light Load)

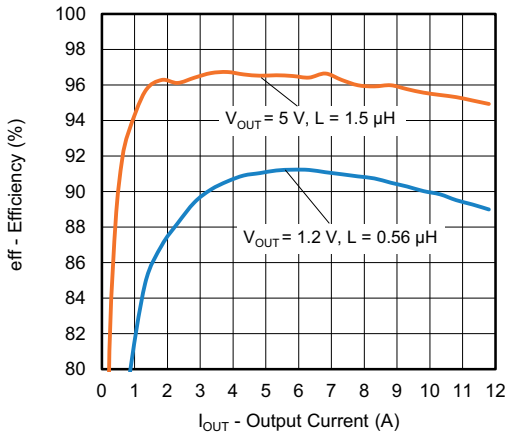


Fig. 17 - SiC437 Efficiency vs. Output Current (VIN = 12 V, fsw = 500 kHz, FCCM, Full Load)

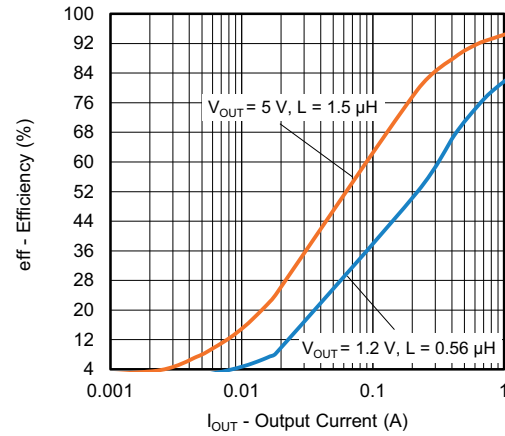


Fig. 20 - SiC437 Efficiency vs. Output Current (VIN = 12 V, fsw = 500 kHz, FCCM, Light Load)

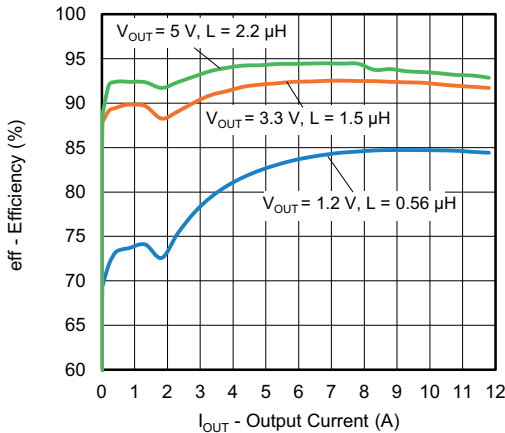


Fig. 18 - SiC437 Efficiency vs. Output Current (VIN = 24 V, fsw = 500 kHz, Full Load)

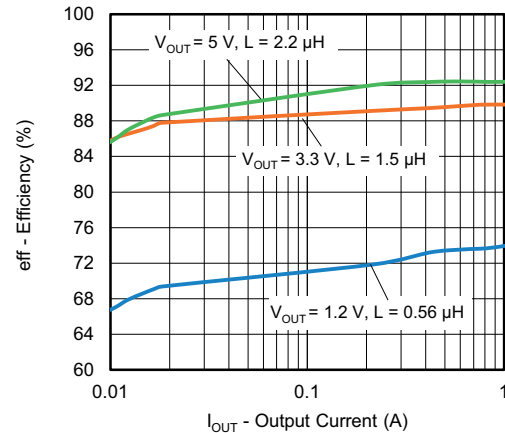


Fig. 21 - SiC437 Efficiency vs. Output Current (VIN = 24 V, fsw = 500 kHz, Light Load)



ELECTRICAL CHARACTERISTICS

(VIN = 12 V, VOUT = 1.2 V, fsw = 500 kHz, COUT = 47 μF x 7, CIN = 10 μF x 6, unless otherwise noted)

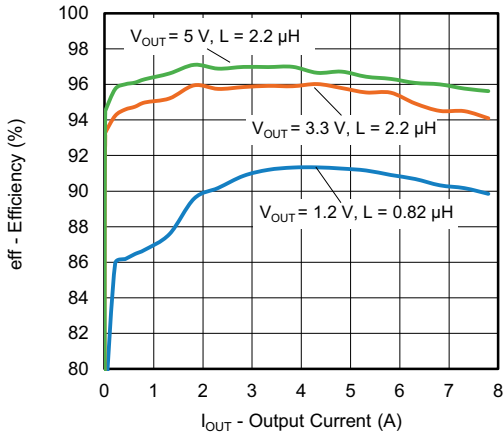


Fig. 22 - SiC438 Efficiency vs. Output Current (VIN = 12 V, fsw = 500 kHz, Full Load)

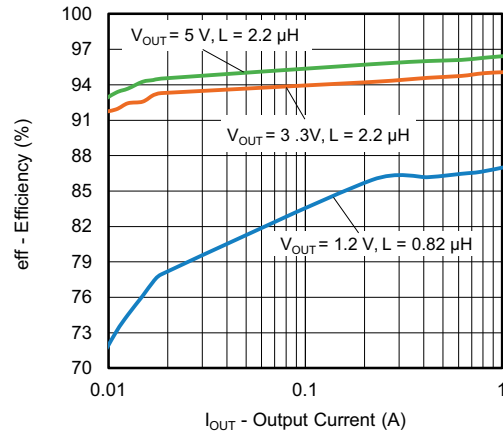


Fig. 25 - SiC438 Efficiency vs. Output Current (VIN = 12 V, fsw = 500 kHz, Light Load)

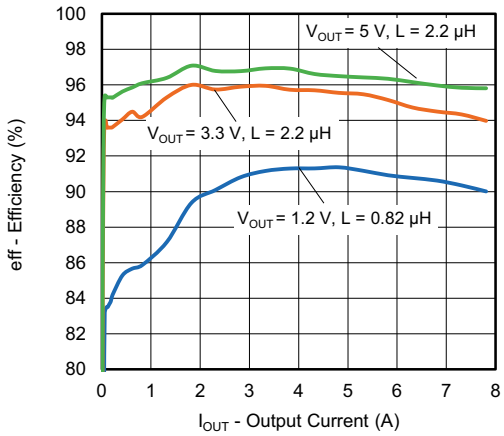


Fig. 23 - SiC438 Efficiency vs. Output Current (VIN = 12 V, fsw = 500 kHz, Ultrasonic Mode, Full Load)

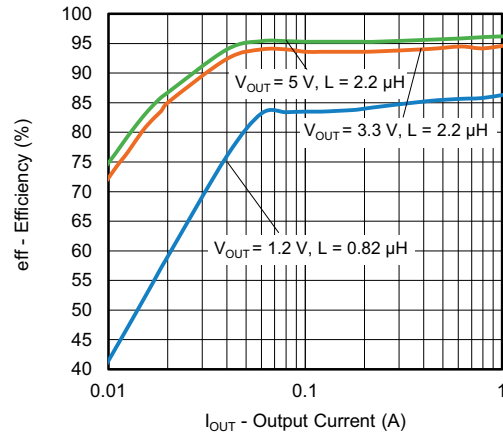


Fig. 26 - SiC438 Efficiency vs. Output Current (VIN = 12 V, fsw = 500 kHz, Ultrasonic Mode, Light Load)

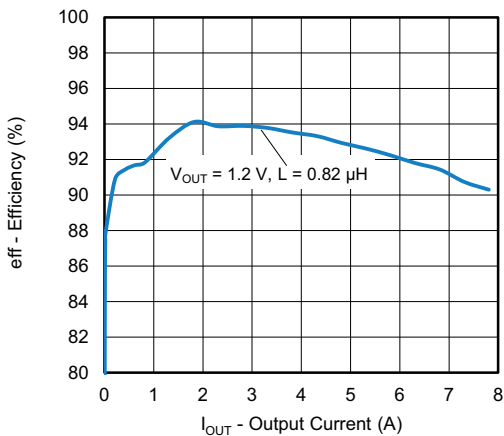


Fig. 24 - SiC438 Efficiency vs. Output Current (VIN = 5 V, fsw = 500 kHz, Full Load)

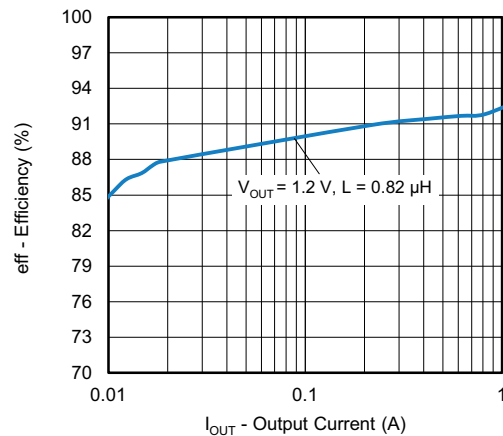


Fig. 27 - SiC438 Efficiency vs. Output Current (VIN = 5 V, fsw = 500 kHz, Light Load)

ELECTRICAL CHARACTERISTICS

($V_{IN} = 12\text{ V}$, $V_{OUT} = 1.2\text{ V}$, $f_{sw} = 500\text{ kHz}$, $C_{OUT} = 47\text{ }\mu\text{F} \times 7$, $C_{IN} = 10\text{ }\mu\text{F} \times 6$, unless otherwise noted)

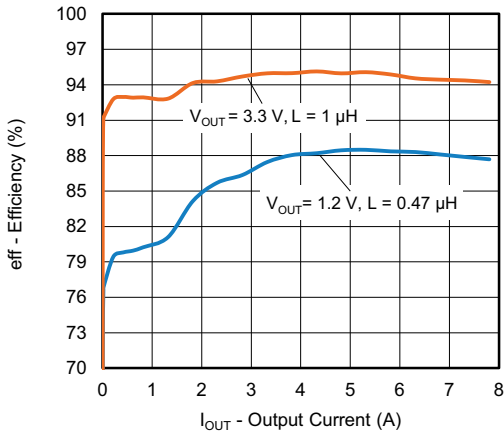


Fig. 28 - SiC438 Efficiency vs. Output Current ($V_{IN} = 12\text{ V}$, $f_{sw} = 1\text{ MHz}$, Full Load)

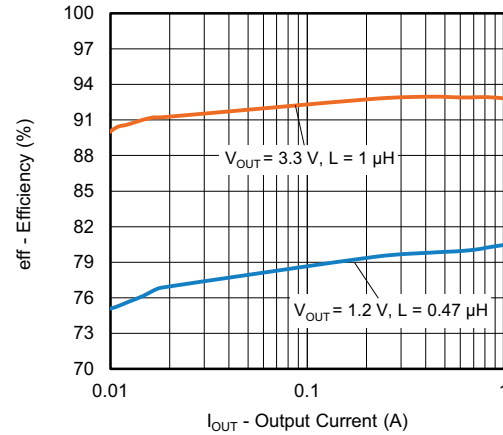


Fig. 31 - SiC438 Efficiency vs. Output Current ($V_{IN} = 12\text{ V}$, $f_{sw} = 1\text{ MHz}$, Light Load)

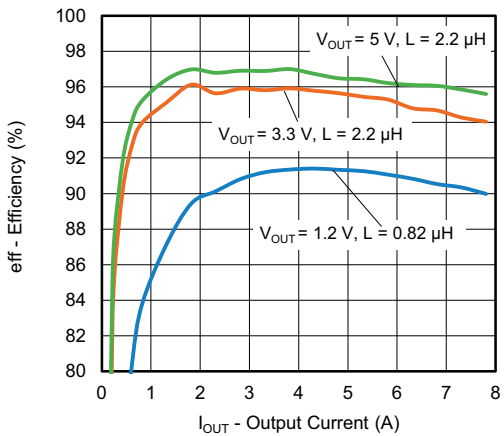


Fig. 29 - SiC438 Efficiency vs. Output Current ($V_{IN} = 12\text{ V}$, $f_{sw} = 500\text{ kHz}$, FCCM, Full Load)

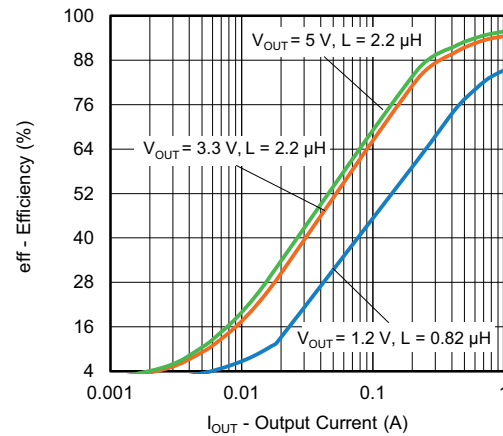


Fig. 32 - SiC438 Efficiency vs. Output Current ($V_{IN} = 12\text{ V}$, $f_{sw} = 500\text{ kHz}$, FCCM, Light Load)

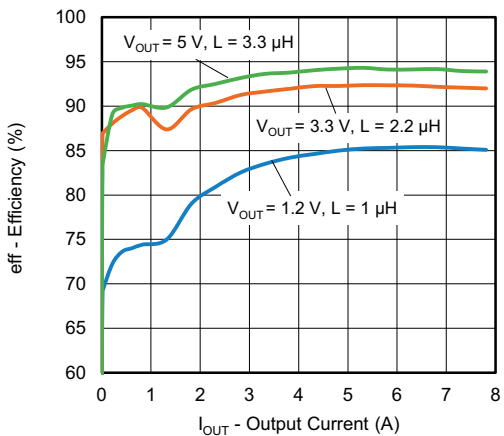


Fig. 30 - SiC438 Efficiency vs. Output Current ($V_{IN} = 24\text{ V}$, $f_{sw} = 500\text{ kHz}$, Full Load)

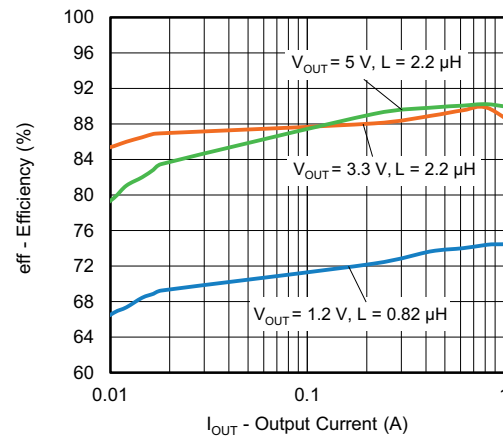


Fig. 33 - SiC438 Efficiency vs. Output Current ($V_{IN} = 24\text{ V}$, $f_{sw} = 500\text{ kHz}$, Light Load)

ELECTRICAL CHARACTERISTICS

($V_{IN} = 12\text{ V}$, $V_{OUT} = 1.2\text{ V}$, $f_{sw} = 500\text{ kHz}$, $C_{OUT} = 47\text{ }\mu\text{F} \times 7$, $C_{IN} = 10\text{ }\mu\text{F} \times 6$, unless otherwise noted)

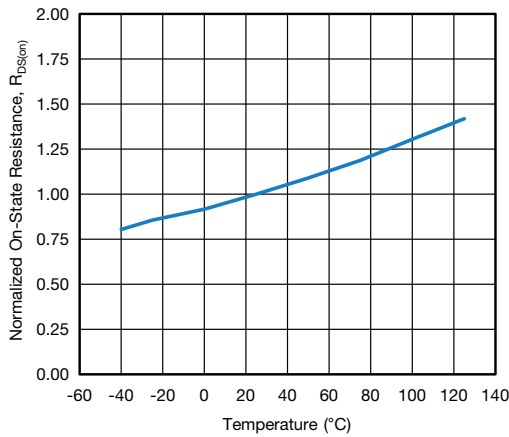


Fig. 34 - On-Resistance vs. Junction Temperature

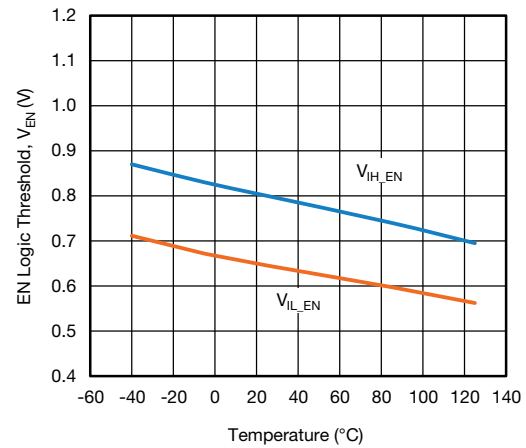


Fig. 37 - EN Logic Threshold vs. Junction Temperature

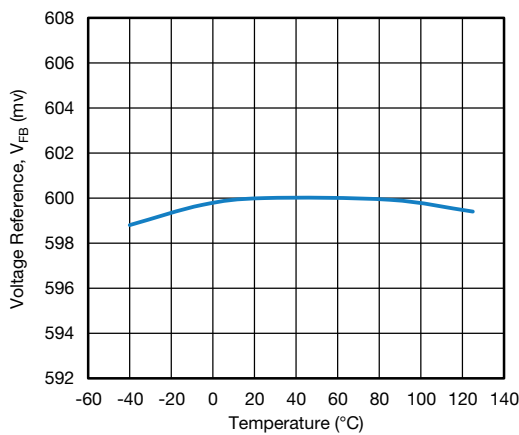


Fig. 35 - Voltage reference vs. Junction Temperature

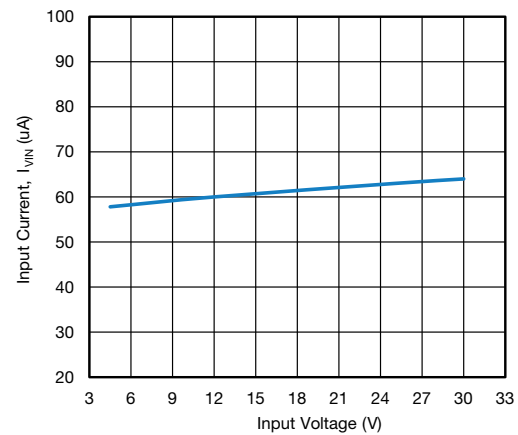


Fig. 38 - Input Current vs. Input Voltage

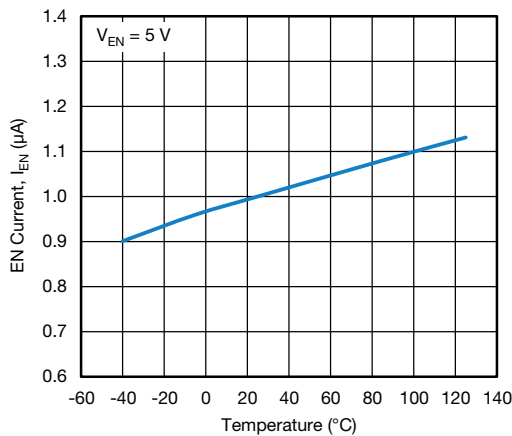


Fig. 36 - EN Current vs. Junction Temperature

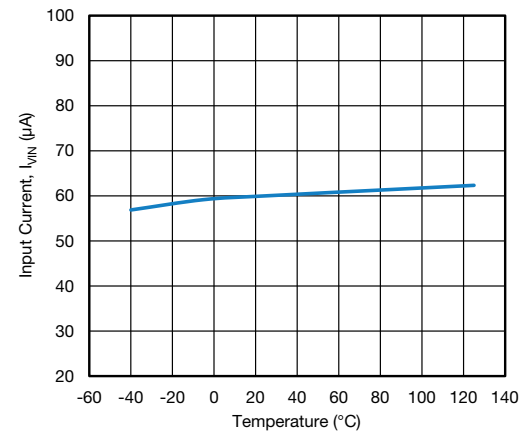


Fig. 39 - Input Current vs. Junction Temperature



ELECTRICAL CHARACTERISTICS

($V_{IN} = 12\text{ V}$, $V_{OUT} = 1.2\text{ V}$, $f_{sw} = 500\text{ kHz}$, $C_{OUT} = 47\text{ }\mu\text{F} \times 7$, $C_{IN} = 10\text{ }\mu\text{F} \times 6$, unless otherwise noted)

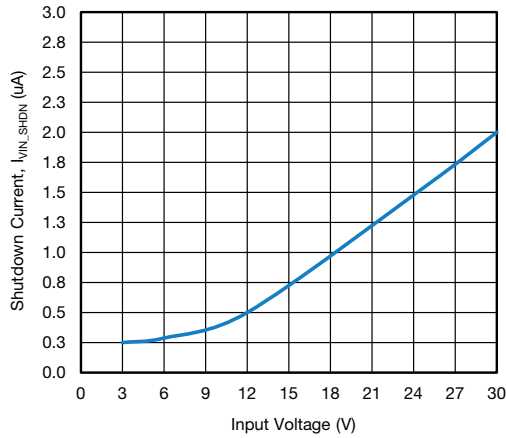


Fig. 40 - Shutdown Current vs. Input Voltage

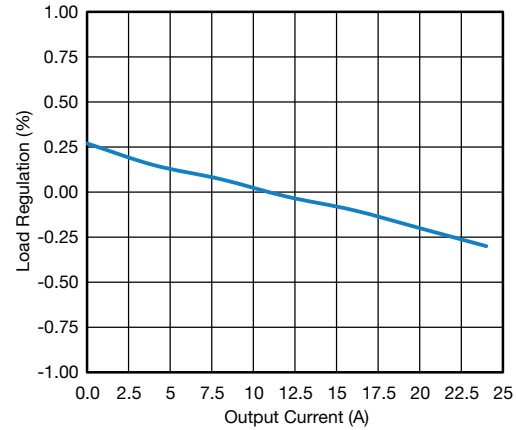


Fig. 42 - Load Regulation vs. Output Current

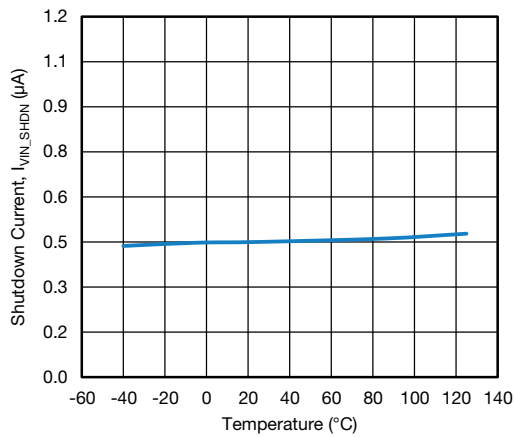


Fig. 41 - Shutdown Current vs. Junction Temperature

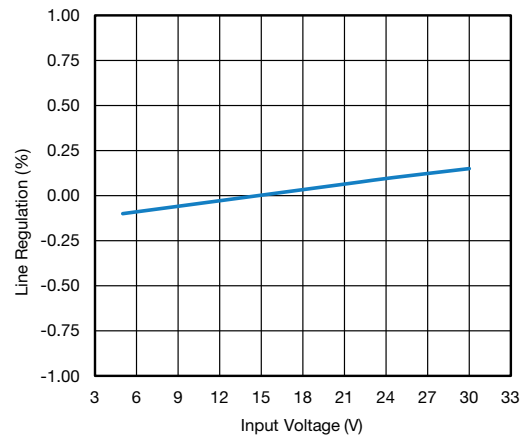
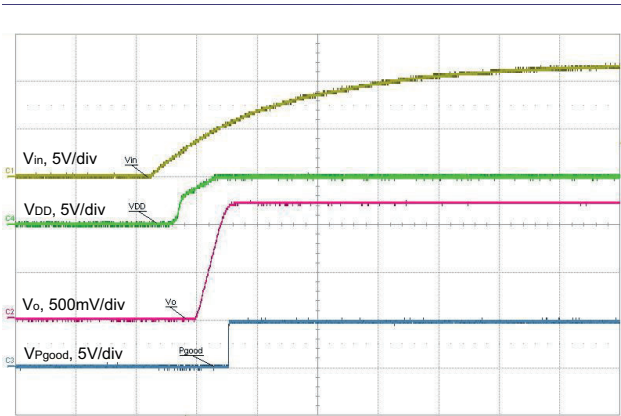
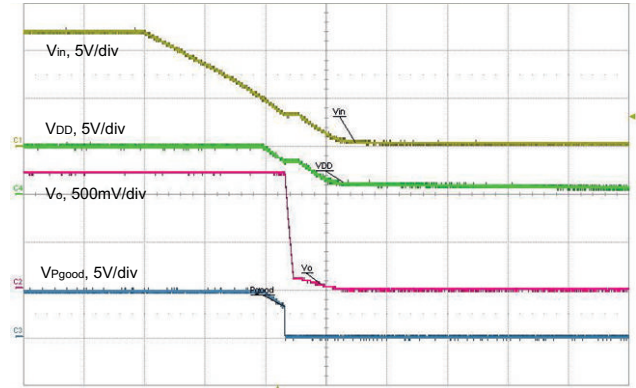
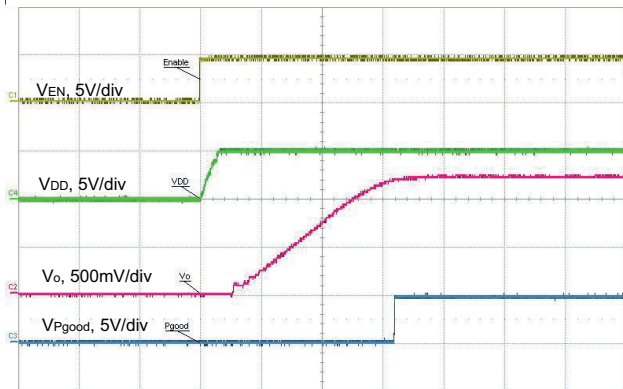
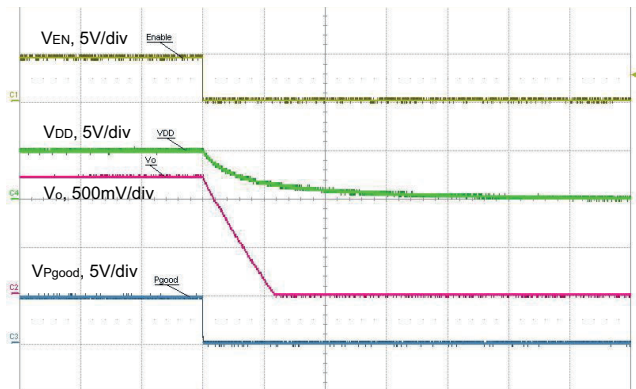
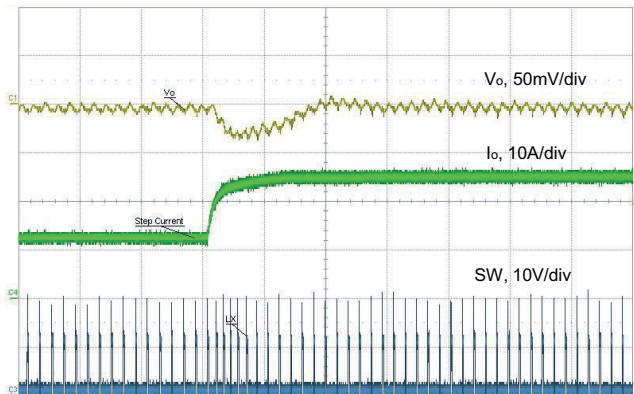
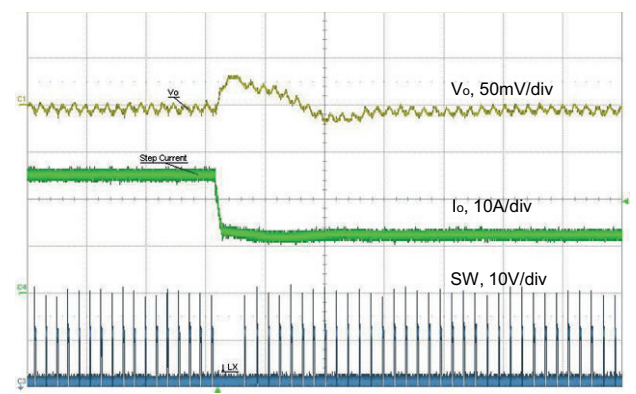


Fig. 43 - Line Regulation vs. Input Voltage

ELECTRICAL CHARACTERISTICS

 ($V_{IN} = 12\text{ V}$, $V_{OUT} = 1.2\text{ V}$, $f_{SW} = 500\text{ kHz}$, $C_{OUT} = 47\text{ }\mu\text{F} \times 7$, $C_{IN} = 10\text{ }\mu\text{F} \times 6$, unless otherwise noted)

Fig. 44 - Startup with V_{IN} , $t = 5\text{ ms/div}$

Fig. 47 - Shut down with V_{IN} , $t = 20\text{ ms/div}$

Fig. 45 - Startup with EN , $t = 1\text{ ms/div}$

Fig. 48 - Shut down with EN , $t = 100\text{ ms/div}$

Fig. 46 - Load Step, 6 A to 12 A, $1\text{ A}/\mu\text{s}$, $t = 10\text{ }\mu\text{s/div}$

Fig. 49 - Load Release, 12 A to 6 A, $1\text{ A}/\mu\text{s}$, $t = 10\text{ }\mu\text{s/div}$

ELECTRICAL CHARACTERISTICS

($V_{IN} = 12\text{ V}$, $V_{OUT} = 1.2\text{ V}$, $f_{sw} = 500\text{ kHz}$, $C_{OUT} = 47\text{ }\mu\text{F} \times 7$, $C_{IN} = 10\text{ }\mu\text{F} \times 6$, unless otherwise noted)

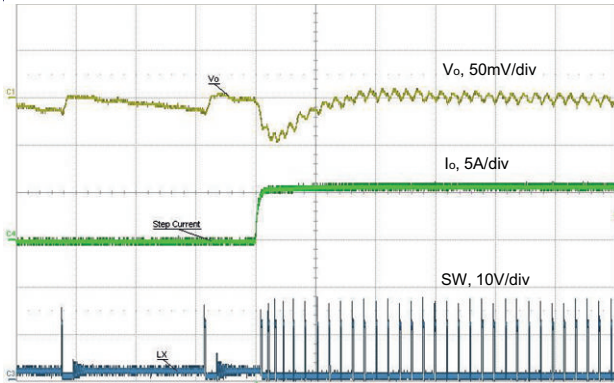


Fig. 50 - Load Step, 0.1 A to 6 A, 1 A/ μ s, $t = 10\text{ }\mu$ s/div Skip Mode Enabled

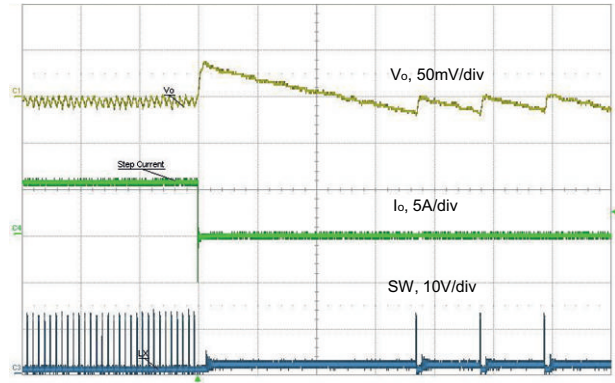


Fig. 53 - Load Release, 6 A to 0.1 A, 1 A/ μ s, $t = 20\text{ }\mu$ s/div Skip Mode Enabled

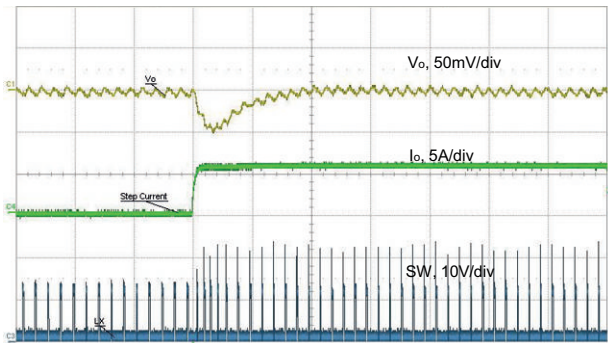


Fig. 51 - Load Step, 0.1 A to 6 A, 1 A/ μ s, $t = 10\text{ }\mu$ s/div Forced Continuous Conduction Mode

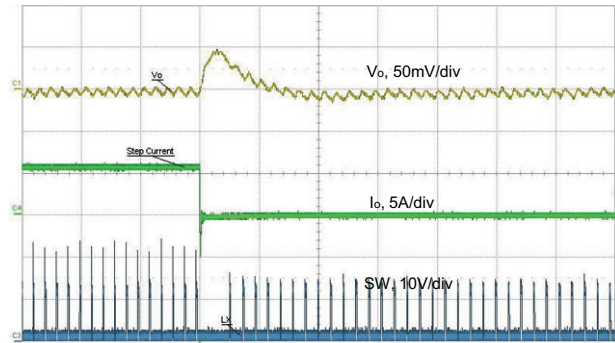


Fig. 54 - Load Release, 6 A to 0.1 A, 1 A/ μ s, $t = 10\text{ }\mu$ s/div Forced Continuous Conduction Mode

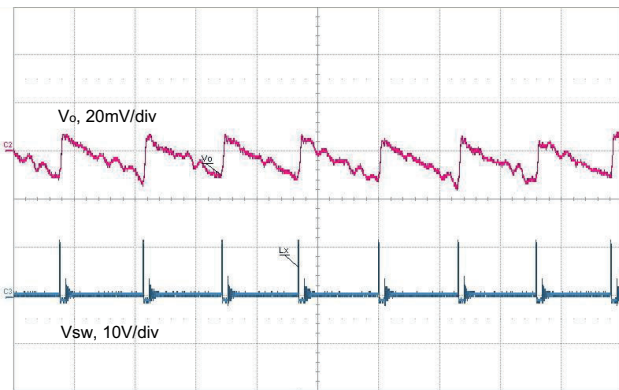


Fig. 52 - Output Ripple, 0.1 A, $t = 20\text{ }\mu$ s/div Skip Mode Enabled

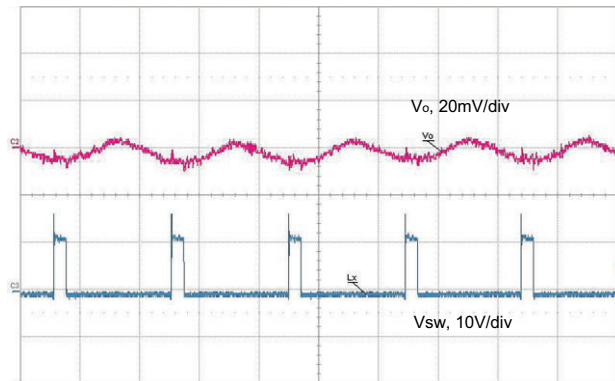
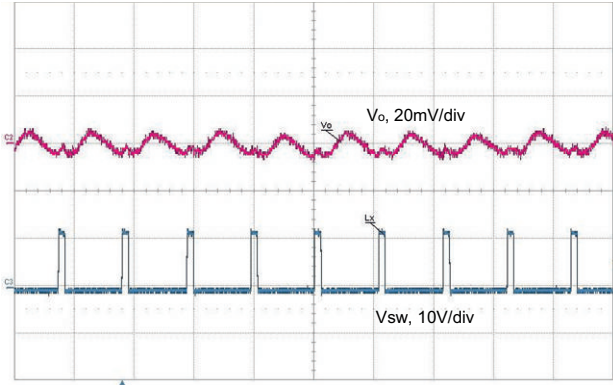


Fig. 55 - Output Ripple, 6 A, $t = 1\text{ }\mu$ s/div Forced Continuous Conduction Mode

ELECTRICAL CHARACTERISTICS

($V_{IN} = 12\text{ V}$, $V_{OUT} = 1.2\text{ V}$, $f_{sw} = 500\text{ kHz}$, $C_{OUT} = 47\text{ }\mu\text{F} \times 7$, $C_{IN} = 10\text{ }\mu\text{F} \times 6$, unless otherwise noted)



**Fig. 56 - Output Ripple, 0.1 A, $t = 2\text{ }\mu\text{s/div}$
Forced Continuous Conduction Mode**

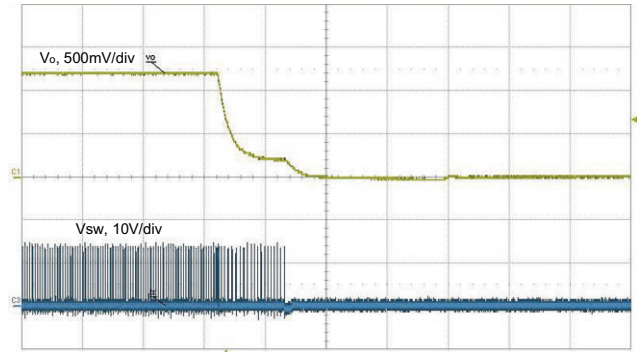


Fig. 58 - Output Undervoltage Protection Behavior, $t = 50\text{ }\mu\text{s/div}$

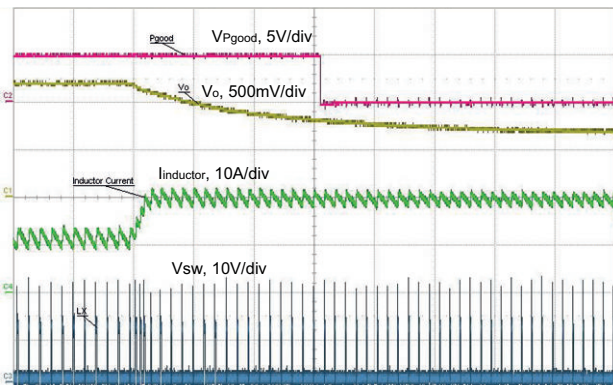


Fig. 57 - Overcurrent Protection Behavior, $t = 10\text{ }\mu\text{s/div}$

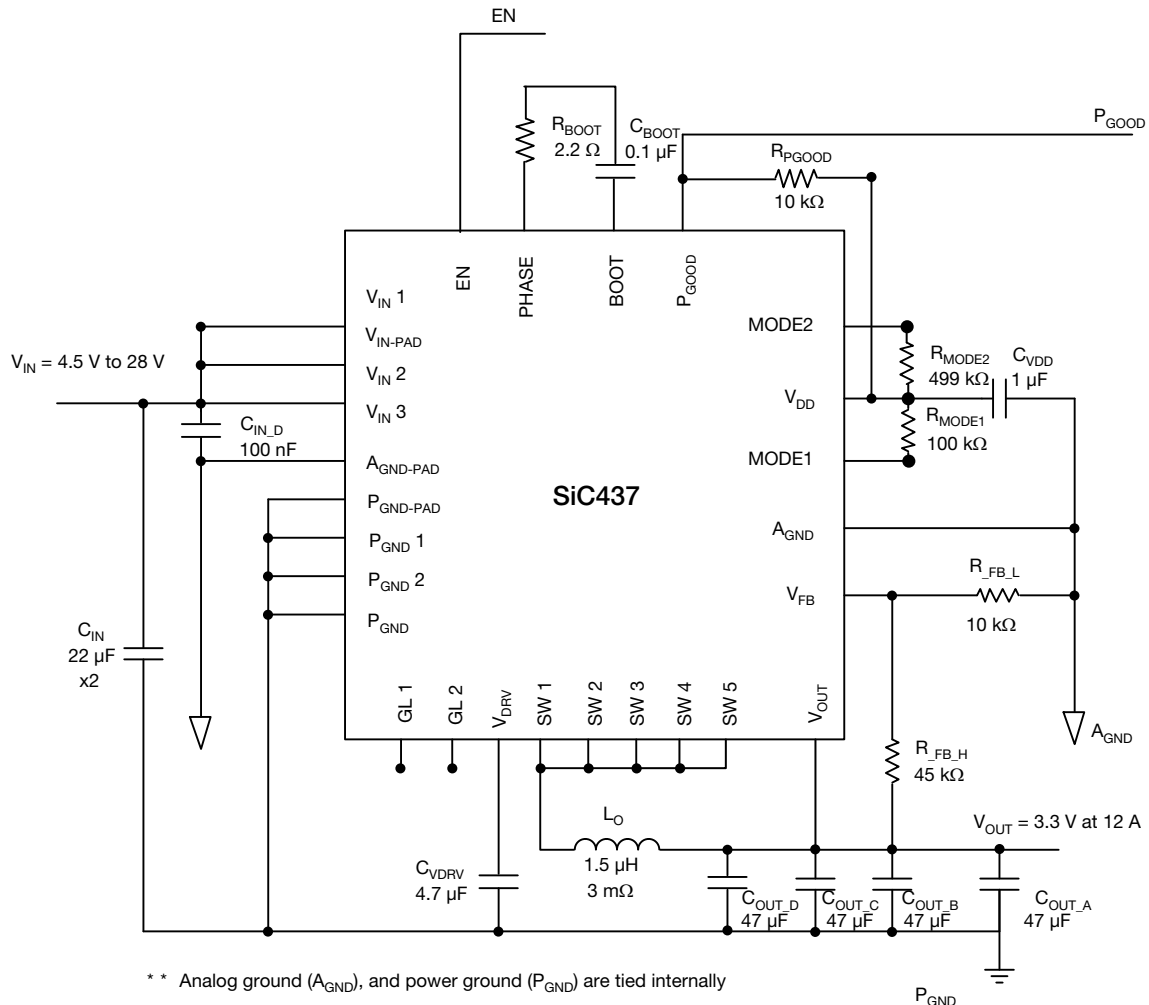
EXAMPLE SCHEMATIC


Fig. 59 - SiC437 configured for 4.5 V to 28 V Input, 3.3 V Output at 12 A, 500 kHz Operating Frequency, Continuous Mode enabled, all Ceramic Output Capacitance Design



EXTERNAL COMPONENT SELECTION FOR THE SiC43X

This section explains external component selection for the SiC43x family of regulators. Component reference designators in any equation refer to the schematic shown in Fig. 59.

See PowerCAD online design center to simplify external component calculations.

Output Voltage Adjustment

If a different output voltage is needed, simply change the value of VOUT and solve for RFB_H based on the following formula:

R_FB_H = (R_FB_L * (V_OUT - V_FB)) / V_FB

Where VFB is 0.6 V for the SiC43X. RFB_L should be a maximum of 10 kΩ to prevent VOUT from drifting at no load.

Inductor Selection

In order to determine the inductance, the ripple current must first be defined. Low inductor values allow for the use of smaller package sizes but create higher ripple current which can reduce efficiency. Higher inductor values will reduce the ripple current and, for a given DC resistance, are more efficient. However, larger inductance translates directly into larger packages and higher cost. Cost, size, output ripple, and efficiency are all used in the selection process.

The ripple current will also set the boundary for power save operation. The SiC431 will typically enter power save mode when the load current decreases to 1/2 of the ripple current. For example, if ripple current is 4 A, power save operation will be active for loads less than 2 A. If ripple current is set at 40 % of maximum load current, power save will typically start at a load which is 20 % of maximum current.

The inductor value is typically selected to provide ripple current of 25 % to 50 % of the maximum load current. This provides an optimal trade-off between cost, efficiency, and transient performance. During the on-time, voltage across the inductor is (VIN - VOUT). The equation for determining inductance is shown below.

LO = ((VIN - VOUT) * D) / (K * IOUT_MAX * fSW)

where, K is the maximum percentage of ripple current, D is the duty cycle, IOUT_MAX is the maximum load current and fSW is the switching frequency.

Capacitor Selection

For instance, the design goal for output voltage ripple is 3 % (45 mV for VOUT = 1.5 V) with ripple current of 4.43 A. The maximum ESR value allowed is shown by the following equation.

The output capacitors are chosen based upon required ESR and capacitance. The maximum ESR requirement is controlled by the output ripple requirement and the DC tolerance. The output voltage has a DC value that is equal to the valley of the output ripple plus 1/2 of the peak-to-peak ripple. A change in the output ripple voltage will lead to a change in DC voltage at the output.

ESR_MAX = (VRIPPLE / IRIPPLE) = (45 mV / 4.43 A)

ESR_MAX = 10.2 mΩ

The output capacitance is usually chosen to meet transient requirements. A worst-case load release (from maximum load to no load) at the moment of peak inductor current, determines the required capacitance. If the load release is instantaneous (maximum load to no load in less than 1 μs) the output capacitor must absorb all the inductor's stored energy. The output capacitor can be calculated according to the following equation.

COUT_MIN = (LO * (IOUT + 0.5 * IRIPPLE_MAX)^2) / (VPK^2 - VOUT^2)

Where IOUT is the output current, IRIPPLE_MAX is the maximum ripple current, VPK is the peak VOUT during load release, VOUT is the output voltage.

The duration of the load release is determined by VOUT and the inductor. During load release, the voltage across the inductor is approximately -VOUT, causing a down-slope or falling di/dt in the inductor. If the di/dt of the load is not much larger than di/dt of the inductor, then the inductor current will tend to track the falling load current. This will reduce the excess inductive energy that must be absorbed by the output capacitor; therefore a smaller capacitance can be used.

Under this circumstance, the following equation can be used to calculate the needed capacitance for a given rate of load release (di_LOAD/dt).

COUT = ((L * IPK^2) / VOUT - (IPK * IRELEASE) * dT) / (2 * (VPK - VOUT) * di_LOAD)

IPK = IRELEASE + (1/2 * IRIPPLE_MAX)



Where I_{PK} is the peak inductor current, I_{RIPPLE_MAX} is the maximum peak to peak inductor current, $I_{RELEASE}$ is the maximum load release current, V_{PK} is the peak V_{OUT} during load release, dI_{LOAD}/dt is the rate of load release.

If the load step does not meet the requirement, increasing the crossover frequency can help by adding feed forward capacitor (C_{FF}) in parallel to the upper feedback resistor to generate another zero and pole. Placing the geometrical mean of this pole and zero around the crossover frequency will result in faster transient response. f_z and f_p are the generated zero and pole, see equations below.

$$f_z = \frac{1}{2\pi \times R_{FB1} \times C_{FF}}$$

$$f_p = \frac{1}{2\pi \times (R_{FB1} // R_{FB2}) \times C_{FF}}$$

Where R_{FB1} is the upper feedback resistor, R_{FB2} is the lower feedback resistor C_{FF} is the feed forward capacitor, f_z is the zero from feed forward capacitor, f_p is the pole frequency generated from the feed forward capacitor.

A calculator is available to assist user to obtain the value of the feed forward capacitance value.

From the calculator, obtain the crossover frequency (f_c). Use the equation below for the calculation of the feed forward capacitance value.

$$f_c = \sqrt{f_z \times f_p}$$

$$C_{FF} = \frac{1}{2\pi \times (f_c \times \sqrt{(R_{FB1} \times (R_{FB1} // R_{FB2}))})}$$

As the internal RC compensation of the SiC431 works with a wide range of output LC filters, the SiC431 offers stable operation for a wide range of output capacitance, making the product versatile and usable in a wide range of applications.

Input Capacitance

In order to determine the minimum capacitance the input voltage ripple needs to be specified; $V_{CINPKPK} \leq 500$ mV is a suitable starting point. This magnitude is determined by the final application specification. The input current needs to be determined for the lowest operating input voltage,

$$I_{CIN(RMS)} = I_O \times \sqrt{D \times (1 - D) + \frac{1}{12} \times \left(\frac{V_{OUT}}{L \times f_{sw} \times I_{OUT}}\right)^2 \times (1 - D)^2 \times D}$$

The minimum input capacitance can then be found,

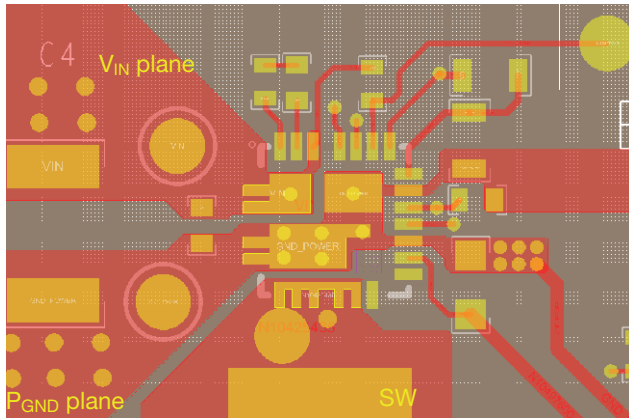
$$C_{IN_min.} = I_{OUT} \times \frac{D \times (1 - D)}{V_{CINPKPK} \times f_{sw}}$$

If high ESR capacitors are used, it is good practice to also add low ESR ceramic capacitance. A 4.7 μ F ceramic input capacitance is a suitable starting point.

Care must be taken to account for voltage derating of the capacitance when choosing an all ceramic input capacitance.

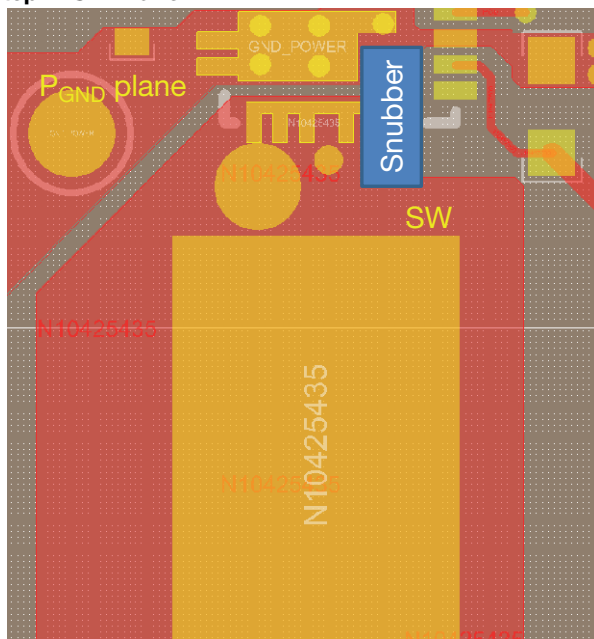
PCB LAYOUT RECOMMENDATIONS

Step 1: V_{IN} /GND Planes and Decoupling



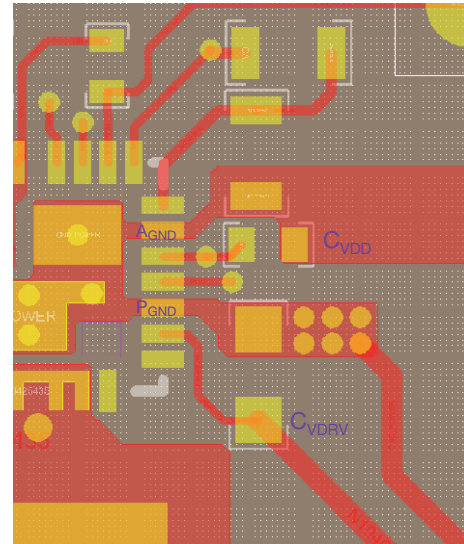
1. Layout V_{IN} and P_{GND} planes as shown above
2. Ceramic capacitors should be placed between V_{IN} and P_{GND} , and very close to the device for best decoupling effect
3. Various ceramic capacitor values and package sizes should be used to cover entire decoupling spectrum e.g. 1210 and 0603
4. Smaller capacitance values, closer to V_{IN} pin(s), provide better high frequency response

Step 2: SW Plane



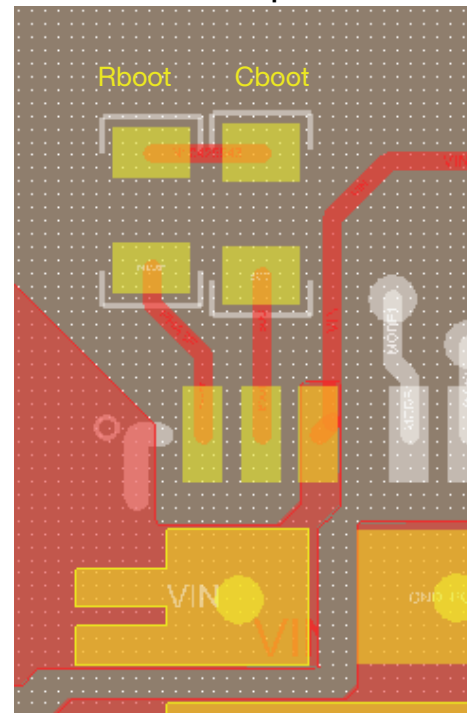
1. Connect output inductor to device with large plane to lower resistance
2. If a snubber network is required, place the components on the bottom layer as shown above

Step 3: V_{DD} / V_{DRV} Input Filter

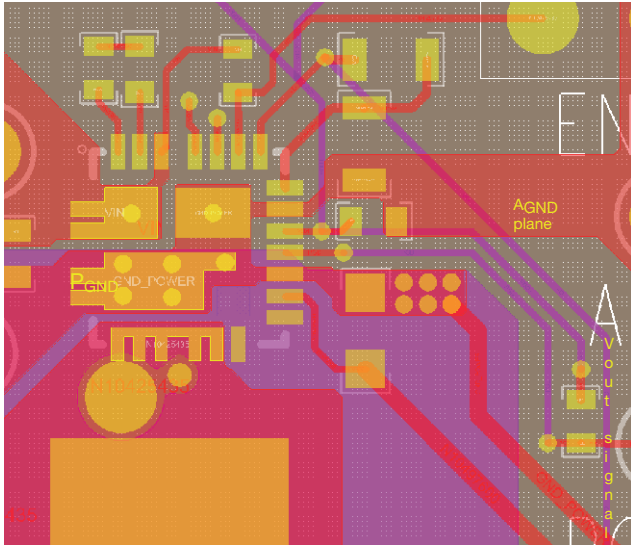


1. C_{VDD} cap should be placed between V_{DD} and A_{GND} to achieve best noise filtering
2. C_{VDRV} cap should be placed close to V_{DRV} and P_{GND} pins to reduce effects of trace impedance and provide maximum instantaneous driver current for low side MOSFET during switching cycle

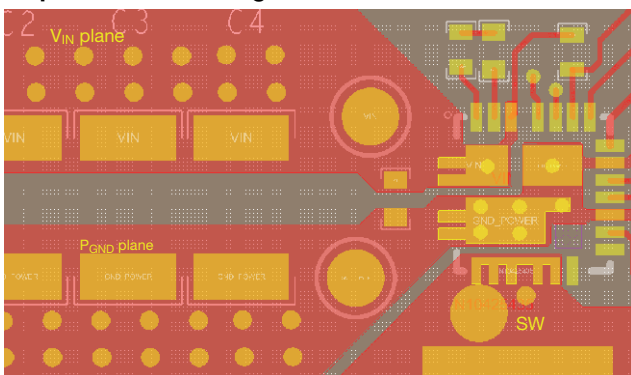
Step 4: BOOT Resistor and Capacitor Placement



1. C_{BOOT} and R_{BOOT} need to be placed very close to the device, between PHASE and BOOT pins
2. In order to reduce parasitic inductance, it is recommended to use 0402 chip size for the resistor and the capacitor

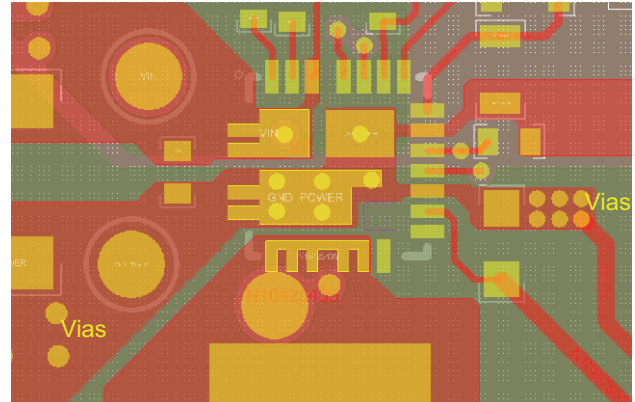
Step 5: Signal Routing


1. Separate the small analog signal from high current path. As shown above, the high paths with high dv/dt , di/dt are placed on the left side of the IC, while the small control signals are placed on the right side of the IC. All the components for small analog signal should be placed closer to IC with minimum trace length
2. IC analog ground (A_{GND}), pin 16, should have a single connection to P_{GND} . The A_{GND} ground plane connected to pin16 helps to keep A_{GND} quiet and improves noise immunity
3. The output signal can be routed through inner layers. Make sure this signal is far away from SW node and shielded by an inner ground layer

Step 6: Thermal Management


1. Thermal relief vias can be added to the V_{IN} and P_{GND} pads to utilize inner layers for high current and thermal dissipation
2. To achieve better thermal performance, additional vias can be placed on V_{IN} and P_{GND} planes. It is also necessary to duplicate the V_{IN} and ground plane at bottom layer to maximize the power dissipation capability of the PCB

3. SW pad is a noise source and it is not recommended to place vias on this pad
4. 8 mil vias on pads and 10 mil vias on planes are ideal via sizes. The vias on pad may drain solder during assembly and cause assembly issues. Please consult with the assembly house for guideline

Step 7: Ground Connection


1. In order to minimize the ground voltage drop due to high current, it is recommended to place vias on the P_{GND} planes. Make use of the inner ground layers to lower the impedance

Step 7: Ground Layer


1. It is recommended to make the whole inner 1 layer (next to top layer) ground plane
2. This ground plane provides shielding between noise source on top layer and signal trace within inner layer
3. The ground plane can be broken into two section, P_{GND} and A_{GND}



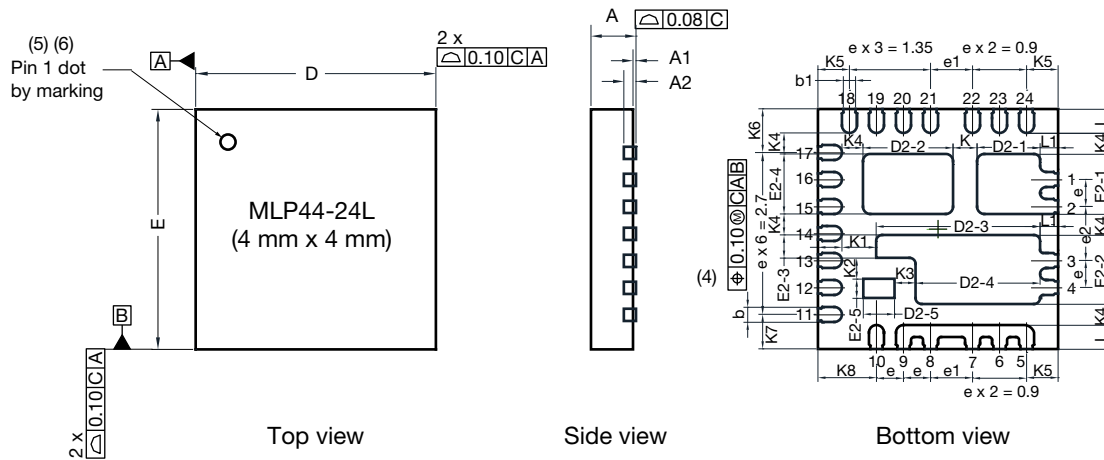
| PRODUCT SUMMARY | | | | |
|-------------------------------|--|--|--|--|
| Part number | SiC437A | SiC437B | SiC437C | SiC437D |
| Description | 12 A, 4.5 V to 28 V input, 300 kHz, 500 kHz, 750 kHz, 1 MHz, synchronous buck regulator with ultrasonic mode and internal 5 V bias | 12 A, 4.5 V to 28 V input, 300 kHz, 500 kHz, 750 kHz, 1 MHz, synchronous buck regulator with power save mode and internal 5 V bias | 12 A, 3 V to 28 V input, 300 kHz, 500 kHz, 750 kHz, 1 MHz, synchronous buck regulator with ultrasonic mode, requires external 5 V bias | 12 A, 3 V to 28 V input, 300 kHz, 500 kHz, 750 kHz, 1 MHz, synchronous buck regulator with power save mode, requires external 5 V bias |
| Input voltage min. (V) | 4.5 | 4.5 | 3 | 3 |
| Input voltage max. (V) | 28 | 28 | 28 | 28 |
| Output voltage min. (V) | 0.6 | 0.6 | 0.6 | 0.6 |
| Output voltage max. (V) | $0.9 \times V_{IN}$ | $0.9 \times V_{IN}$ | $0.9 \times V_{IN}$ | $0.9 \times V_{IN}$ |
| Continuous current (A) | 12 | 12 | 12 | 12 |
| Switch frequency min. (kHz) | 300 | 300 | 300 | 300 |
| Switch frequency max. (kHz) | 1000 | 1000 | 1000 | 1000 |
| Pre-bias operation (yes / no) | Yes | Yes | Yes | Yes |
| Internal bias reg. (yes / no) | Yes | Yes | No | No |
| Compensation | Internal | Internal | Internal | Internal |
| Enable (yes / no) | Yes | Yes | Yes | Yes |
| P _{GOOD} (yes / no) | Yes | Yes | Yes | Yes |
| Over current protection | Yes | Yes | Yes | Yes |
| Protection | OVP, OCP, UVP/SCP, OTP, UVLO | OVP, OCP, UVP/SCP, OTP, UVLO | OVP, OCP, UVP/SCP, OTP, UVLO | OVP, OCP, UVP/SCP, OTP, UVLO |
| Light load mode | Selectable ultrasonic | Selectable powersave | Selectable ultrasonic | Selectable powersave |
| Peak efficiency (%) | 97 | 97 | 97 | 97 |
| Package type | PowerPAK MLP44-24L | PowerPAK MLP44-24L | PowerPAK MLP44-24L | PowerPAK MLP44-24L |
| Package size (W, L, H) (mm) | 4 x 4 x 0.75 | 4 x 4 x 0.75 | 4 x 4 x 0.75 | 4 x 4 x 0.75 |
| Status code | 1 | 1 | 1 | 1 |
| Product type | microBUCK (step down regulator) | microBUCK (step down regulator) | microBUCK (step down regulator) | microBUCK (step down regulator) |
| Applications | Computing, consumer, industrial, healthcare, networking | Computing, consumer, industrial, healthcare, networking | Computing, consumer, industrial, healthcare, networking | Computing, consumer, industrial, healthcare, networking |



| PRODUCT SUMMARY | | | | |
|-------------------------------|---|---|---|---|
| Part number | SiC438A | SiC438B | SiC438C | SiC438D |
| Description | 8 A, 4.5 V to 28 V input, 300 kHz, 500 kHz, 750 kHz, 1 MHz, synchronous buck regulator with ultrasonic mode and internal 5 V bias | 8 A, 4.5 V to 28 V input, 300 kHz, 500 kHz, 750 kHz, 1 MHz, synchronous buck regulator with power save mode and internal 5 V bias | 8 A, 3 V to 28 V input, 300 kHz, 500 kHz, 750 kHz, 1 MHz, synchronous buck regulator with ultrasonic mode, requires external 5 V bias | 8 A, 3 V to 28 V input, 300 kHz, 500 kHz, 750 kHz, 1 MHz, synchronous buck regulator with power save mode, requires external 5 V bias |
| Input voltage min. (V) | 4.5 | 4.5 | 3 | 3 |
| Input voltage max. (V) | 28 | 28 | 28 | 28 |
| Output voltage min. (V) | 0.6 | 0.6 | 0.6 | 0.6 |
| Output voltage max. (V) | 0.9 x V _{IN} | 0.9 x V _{IN} | 0.9 x V _{IN} | 0.9 x V _{IN} |
| Continuous current (A) | 8 | 8 | 8 | 8 |
| Switch frequency min. (kHz) | 300 | 300 | 300 | 300 |
| Switch frequency max. (kHz) | 1000 | 1000 | 1000 | 1000 |
| Pre-bias operation (yes / no) | Yes | Yes | Yes | Yes |
| Internal bias reg. (yes / no) | Yes | Yes | No | No |
| Compensation | Internal | Internal | Internal | Internal |
| Enable (yes / no) | Yes | Yes | Yes | Yes |
| P _{GOOD} (yes / no) | Yes | Yes | Yes | Yes |
| Overcurrent protection | Yes | Yes | Yes | Yes |
| Protection | OVP, OCP, UVP/SCP, OTP, UVLO | OVP, OCP, UVP/SCP, OTP, UVLO | OVP, OCP, UVP/SCP, OTP, UVLO | OVP, OCP, UVP/SCP, OTP, UVLO |
| Light load mode | Selectable ultrasonic | Selectable powersave | Selectable ultrasonic | Selectable powersave |
| Peak efficiency (%) | 97 | 97 | 97 | 97 |
| Package type | PowerPAK MLP44-24L | PowerPAK MLP44-24L | PowerPAK MLP44-24L | PowerPAK MLP44-24L |
| Package size (W, L, H) (mm) | 4 x 4 x 0.75 | 4 x 4 x 0.75 | 4 x 4 x 0.75 | 4 x 4 x 0.75 |
| Status code | 2 | 2 | 2 | 2 |
| Product type | microBUCK (step down regulator) | microBUCK (step down regulator) | microBUCK (step down regulator) | microBUCK (step down regulator) |
| Applications | Computing, consumer, industrial, healthcare, networking | Computing, consumer, industrial, healthcare, networking | Computing, consumer, industrial, healthcare, networking | Computing, consumer, industrial, healthcare, networking |

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PowerPAK[®] MLP44-24L Case Outline



| DIM. | MILLIMETERS | | | INCHES | | |
|------------------|-------------|------|------|------------|-------|-------|
| | MIN. | NOM. | MAX. | MIN. | NOM. | MAX. |
| A ⁽⁸⁾ | 0.70 | 0.75 | 0.80 | 0.027 | 0.029 | 0.031 |
| A1 | 0.00 | - | 0.05 | 0.000 | - | 0.002 |
| A2 | 0.20 ref. | | | 0.008 ref. | | |
| b ⁽⁴⁾ | 0.20 | 0.25 | 0.30 | 0.008 | 0.010 | 0.012 |
| b1 | 0.15 | 0.20 | 0.25 | 0.006 | 0.008 | 0.010 |
| D | 3.90 | 4.00 | 4.10 | 0.155 | 0.157 | 0.159 |
| e | 0.45 BSC | | | 0.018 BSC | | |
| e1 | 0.70 BSC | | | 0.028 BSC | | |
| e2 | 0.90 BSC | | | 0.035 BSC | | |
| E | 3.90 | 4.00 | 4.10 | 0.154 | 0.157 | 0.161 |
| L | 0.35 | 0.40 | 0.45 | 0.014 | 0.016 | 0.018 |
| N ⁽³⁾ | 24 | | | 24 | | |
| D2-1 | 1.00 | 1.05 | 1.10 | 0.039 | 0.041 | 0.043 |
| D2-2 | 1.45 | 1.50 | 1.55 | 0.057 | 0.059 | 0.061 |
| D2-3 | 2.68 | 2.73 | 2.78 | 0.106 | 0.108 | 0.110 |
| D2-4 | 2.02 | 2.07 | 2.12 | 0.079 | 0.081 | 0.083 |
| D2-5 | 0.47 | 0.52 | 0.57 | 0.018 | 0.020 | 0.022 |
| E2-1 | 0.95 | 1.00 | 1.05 | 0.037 | 0.039 | 0.041 |
| E2-2 | 1.10 | 1.15 | 1.20 | 0.043 | 0.045 | 0.047 |
| E2-3 | 0.33 | 0.38 | 0.43 | 0.013 | 0.015 | 0.017 |
| E2-4 | 0.95 | 1.00 | 1.05 | 0.037 | 0.039 | 0.041 |
| E2-5 | 0.27 | 0.32 | 0.37 | 0.011 | 0.013 | 0.015 |
| K | 0.40 ref. | | | 0.016 ref. | | |
| K1 | 0.57 ref. | | | 0.022 ref. | | |
| K2 | 0.35 ref. | | | 0.014 ref. | | |
| K3 | 0.35 ref. | | | 0.014 ref. | | |
| K4 | 0.35 ref. | | | 0.014 ref. | | |
| K5 | 0.525 ref. | | | 0.021 ref. | | |
| K6 | 0.725 ref. | | | 0.029 ref. | | |
| K7 | 0.575 ref. | | | 0.023 ref. | | |
| K8 | 0.975 ref. | | | 0.038 ref. | | |

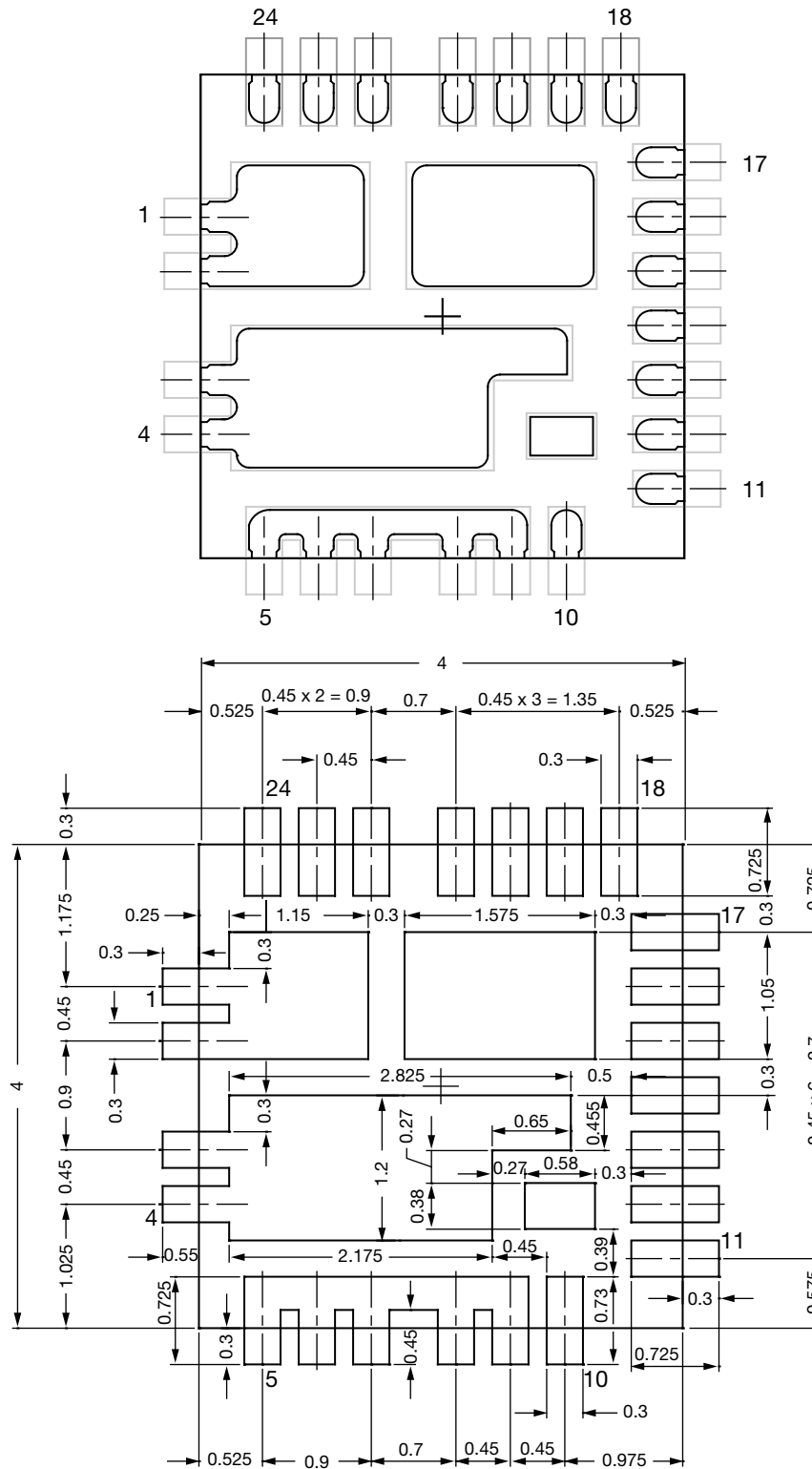
ECN: T17-0551-Rev. B, 16-Oct-17
DWG: 6055

Notes

- (1) Use millimeters as the primary measurement
- (2) Dimensioning and tolerances conform to ASME Y14.5M. - 1994
- (3) N is the number of terminals
- (4) Dimension b applies to plated terminal and is measured between 0.20 mm and 0.25 mm from terminal tip
- (5) The pin #1 identifier must be existed on the top surface of the package by using indentation mark or other feature of package body
- (6) Exact shape and size of this feature is optional
- (7) Package warpage max. 0.08 mm
- (8) Applied only for terminals



Recommended Land Pattern PowerPAK® MLP44-24L



All dimensions are in millimeters



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